ST1S03 alternative topology:
Using a buck in a negative buck-boost configuration

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By Nicola Siciliano

<table>
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<th>Main components</th>
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<td>ST1S03</td>
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**Specification**

- ST1S03 (Buck regulator) in buck-boost configuration
- Vin=3.3V,
- Vout=-5V,
- Iout up to -500mA

**Circuit description: From a buck to a buck-boost**

1) **Buck topology**: Basic Working Principle in Continuous Conduction Mode

The schematic in Figure 1 shows the ST1S03 configured as a step-down converter. The Vout is adjustable through the external resistor divider R1 and R2 according to the following equation:

\[ V_{OUT} = V_{FB} \left[ 1 + \frac{R_1}{R_2} \right] \]

with a duty cycle of \( D = \frac{V_{out}}{V_{in}} \).

During \( T_{ON} \), the internal switch (between Vin-SW and SW) is ON and the inductor \( L_1 \) is connected between \( V_{in} \) and \( V_{OUT} \). The inductor current \( (i_L) \) rate of change is given by:

\[ \frac{di}{dt} = \frac{Vin - Vout}{L} \]

During \( T_{OFF} \), the inductor starts to release the energy (stored during \( T_{ON} \)) so the voltage across it changes polarity to keep the current flowing in the same direction. Assuming for simplicity the voltage drop across diode D1 is negligible, the inductor current ramps down at a rate of:
\[
\frac{di}{dt} = \frac{V_{out}}{L}.
\]

The steady-state load current is always carried by the inductor during both ON and OFF times. The average inductor current is equal to the load current, and the peak-to-peak inductor ripple current is

\[
I_{L(PP)} = \frac{(Vin - Vout)D}{f_{SW}L}
\]

where \(f_{SW}\) is the switching frequency, which is 1.5MHz for the ST1S03.

**Figure 1.** ST1S03 in Step-Down (Buck) configuration

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2) **Alternative Buck-boost topology: Basic Working Principle in Continuous Conduction Mode**

Starting from the application schematic in Figure 1, it is possible, with only a few adjustments, to switch from a buck configuration to an inverting buck-boost configuration.

The new schematic is shown in Figure 2. Compared to the buck configuration, the main differences are:

1) Device GND (pin2) is connected to the Output, which is the point at the lowest potential in the application.
2) The Schottky diode D1 is reversed, with the cathode toward the device and the anode toward Vout.
3) The inductor L1 is tied to the GND of the system.
4) Capacitor C3 is added between Vin and Vout as a bypass capacitor across the device voltage input (pin2 and pin 4).
At power-up \( t_0 \) of the Vcc ramp-up, the device GND (pin2) is at the same potential as the GND system \( (V_{out}=0V) \). Once the input voltage rises above 2.5V, the circuit starts switching, energizing the inductor. Vout then starts to increase “negatively”, until the drop across R1 reaches 0.8V above Vout.

The output voltage is still determined by the resistors divider R1 and R2, according to the equation:

\[
|V_{\text{out}}| = V_{FB} \left[ 1 + \frac{R_1}{R_2} \right]
\]

But in this case, Vout is negative. With a duty cycle of:

\[
D = \frac{|V_{\text{out}}|}{V_{\text{in}} + |V_{\text{out}}|}
\]

During \( T_{ON} \), the internal switch (between Vin-SW and SW) is ON, so the inductor L1 is connected between VIN and GND, and the inductor current \( (i_L) \) rate of change is given by:

\[
\frac{di}{dt} = \frac{V_{\text{in}}}{L}
\]

During this phase, only the output capacitor C2 provides the output current.

At \( T_{OFF} \) (internal switch is off), the inductor starts to release the energy stored during \( T_{ON} \) so the voltage across it changes polarity to keep the current flowing in the same direction. The voltage across the inductor becomes approximately VOUT, and the inductor current decreases at a rate of:
\[
\frac{di}{dt} = \frac{-V_{out}}{L}.
\]

During $T_{OFF}$ the inductor supplies current to the load and also replenishes the energy lost by the capacitor during $T_{ON}$. For the buck-boost circuit, the average inductor current is:

\[
I_{L(\text{avg})} = \frac{I_{out}}{1-D}
\]

and the peak-to-peak inductor current is:

\[
I_{L(\text{PP})} = \frac{V_{in}D}{f_{SW}L}.
\]

The average inductor current cannot exceed the average rated current of the switching regulator ($I_{SW}$); therefore the buck-boost output current is reduced by a factor of $1-D$. In this configuration, the maximum available DC output current is:

\[
I_{OUT} = I_{SW}(1-D).
\]

and, the ST1S03 rated current ($I_{SW}$) is 1.5A.

These basic differences between the two circuits’ functionality must be taken into consideration when a buck converter IC is used as a buck-boost converter.

3) Input Voltage and output current

In the buck-boost topology of Figure 2, the ST1S03 ground pin is connected to $V_{OUT}$. Therefore the voltage across the device is $V_{IN} + |V_{OUT}|$, rather than just $V_{IN}$ as in the buck topology. The differential between the two voltages cannot exceed the ST1S03 maximum rating of 16V.

\[
V_{IN} + |V_{OUT}| < 16V
\]

In addition, a minimum $V_{IN} = 3V$ it is needed to guarantee the application start-up.

The current capability depends on the application’s input and output voltages, which dictate the duty cycle and therefore the maximum output current.

**Measurement results**

The suggested buck-boost topology (based on ST1S03) was tested using the schematic in Figure 2. The waveforms in Figure 3 show a typical behavior under the following conditions:
- Vin = 3.3V
- Vout = -5V
- Iout = -500mA

**Figure 3.** Buck-Boost waveforms @ Vin = 3.3V, Vout = -5V, Iout = -500mA

- Channel 1 (yellow) is Vin = 3.3V
- Channel 2 (black) is the inductor current; 1.7A max
- Channel 3 (green) is the switching node (pin 3 on the ST1S03), duty-cycle 66%
- Channel 4 (light blue) is Vout = -5.0V
- A (purple) is Iout = -500mA

The test results show the impact of the losses due to the ST1S03, diode and the additional components, which are not accounted for in the formulas here presented (Table 1).

**Consideration**

When an asynchronous buck converter such as the ST1S03 is used in an inverting buck-boost configuration, certain considerations must be made. The basic design equations of the two topologies presented here are collected in Table 1. These equations address the continuous conduction mode in simplified form because they assume the losses on the semiconductors and other components are negligible.
Table 1. Basic design equations in continuous conduction mode

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<thead>
<tr>
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<th>Buck</th>
<th>Buck-boost</th>
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<tbody>
<tr>
<td>Duty cycle</td>
<td>$D = \frac{V_{out}}{Vin}$</td>
<td>$D = \frac{</td>
</tr>
<tr>
<td>Average inductor current</td>
<td>$I_{L(avg)} = I_{out}$</td>
<td>$I_{L(avg)} = \frac{I_{out}}{1 - D}$</td>
</tr>
<tr>
<td>Peak-to-peak inductor ripple current</td>
<td>$I_{L(PP)} = \frac{(Vin - Vout)D}{f_{SW}L}$</td>
<td>$I_{L(PP)} = \frac{VinD}{f_{SW}L}$</td>
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<tr>
<td>Ramp-up inductor current</td>
<td>$\frac{di}{dt} = \frac{Vin - Vout}{L}$</td>
<td>$\frac{di}{dt} = \frac{Vin}{L}$</td>
</tr>
<tr>
<td>Ramp-down inductor current</td>
<td>$\frac{di}{dt} = \frac{Vout}{L}$</td>
<td>$\frac{di}{dt} = -\frac{Vout}{L}$</td>
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Variations

The following are some of the ST asynchronous buck regulators that can be configured as negative buck-boost:

- L497x family
- L597x family
- L5980, 1, 3, 5, 6 & 7
- L798x family

Support material

- **Product Evaluation board:**
  - STEVAL-ISA042V2: 1.5 A / 3.3 V step-down DC-DC converter demonstration board based on the ST1S03
  - STEVAL-ISA042V1: 1.5 A / 1.2 V step-down DC-DC converter demonstration board based on the ST1S03

- **Datasheet** – ST1S03: 1.5 A, 1.5 MHz adjustable, step-down switching regulator

- **Application note:**
  - AN2093: ST1S03 buck converters for HDD power supplies
  - AN2837: Positive to negative buck-boost converter using ST1S03 asynchronous switching regulator

Revision history

<table>
<thead>
<tr>
<th>Date</th>
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<tbody>
<tr>
<td>30-Aug-2012</td>
<td>1</td>
<td>Initial release</td>
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