

# Designing Low Power SMPS with VIPerPlus Family of Products

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**ST Developers  
Conference**

September 12th, 2019  
Santa Clara Convention Center - Mission City Ballroom  
Santa Clara, CA



- Flyback Topology
- Buck Topology
- eDesignSuite Examples



# Introduction

## Auxiliary Power Supply

Major Appliances



Air conditioning



Industrials



Lighting



Electrical Vehicle



## Main Power Supply

Smart Meters



Smart Buildings



Small Industrials



Small Appliances



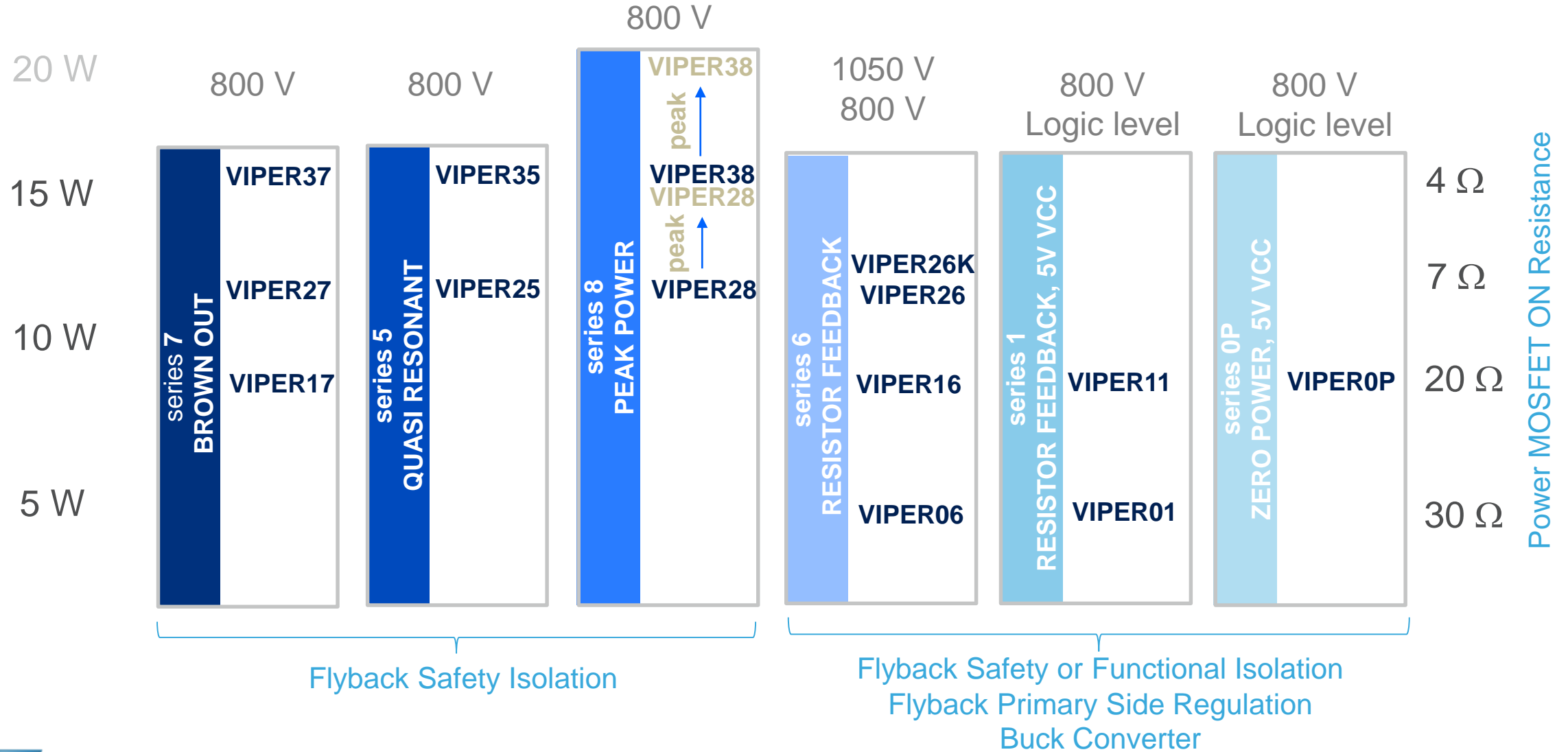
Adapters



# Products

5

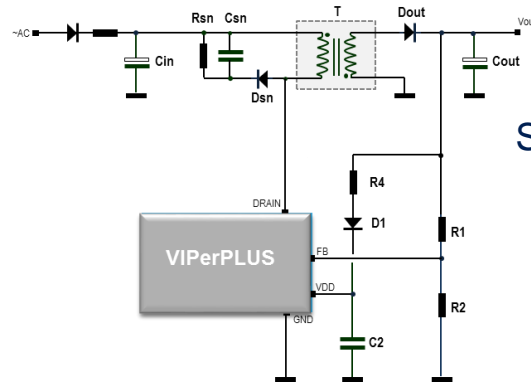
Output Power @ 85-265 VAC Input Voltage



# Which Topology?

6

## Functional Isolation (Not Isolated Galvanically)



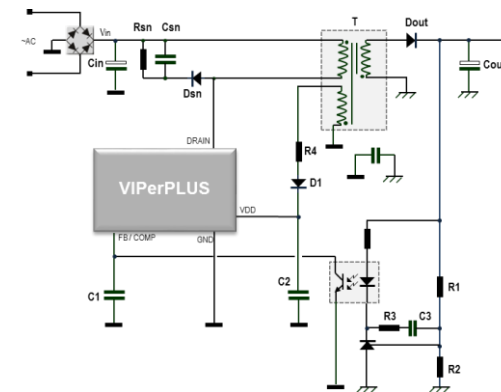
Secondary Regulation  
with Resistor Divider

Flyback  
Converter

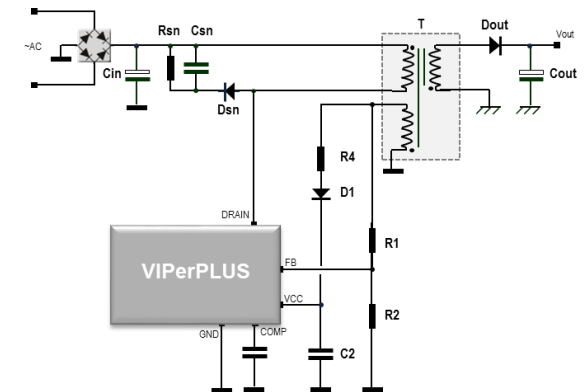


## Galvanic Isolation For Touchable Outputs

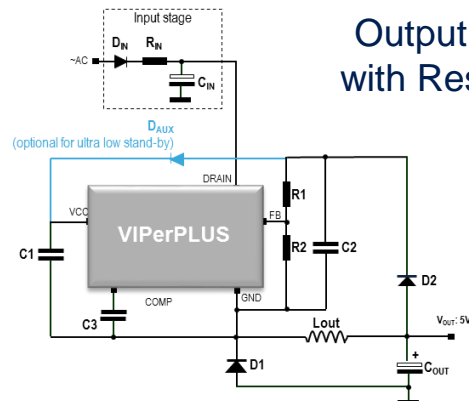
Secondary-Side Regulation  
With Opto-Coupler For Tight Regulation



Primary-Side Regulation  
Without Opto-Coupler



## Buck Non-Isolated



Output Regulation  
with Resistor Divider

Buck Converter  
Small Inductor  
Compact PCB

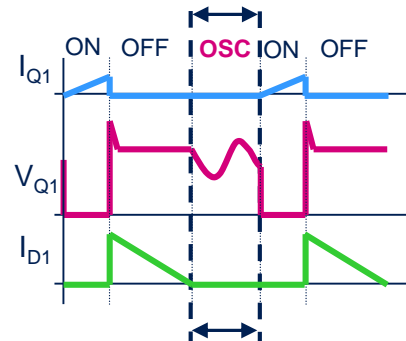
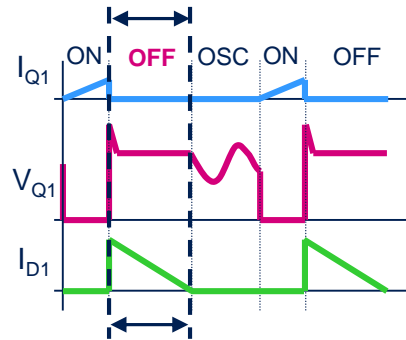
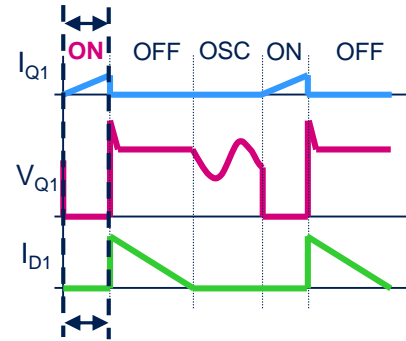
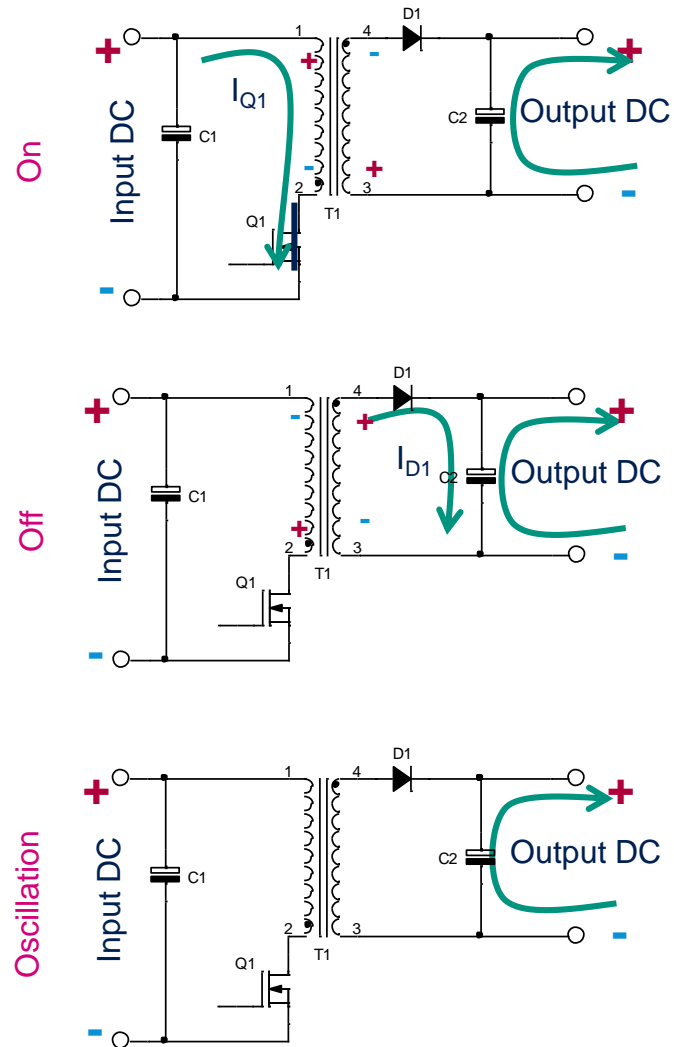




# Flyback Topology Optimization

# Flyback Operation

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$$E_{T1} = \frac{1}{2} L_P I_{Q1PK}^2$$

$$P_{T1} = \frac{1}{2} L_P I_{Q1PK}^2 f_{SW}$$

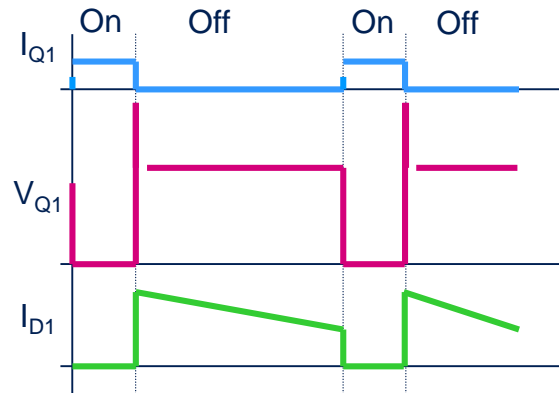
$$I_{D1PK} = \frac{N_P}{N_S} I_{Q1PK} = n_{T1} I_{Q1PK}$$

$$E_{T1} = \frac{1}{2} L_S I_{D1PK}^2$$

$$L_S = \frac{L_P}{n_{T1}^2}$$

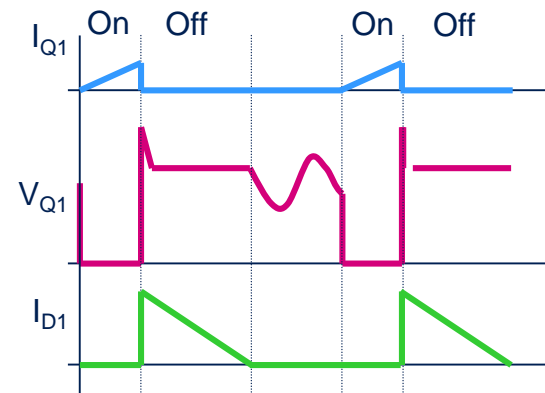


## Continuous Mode (CCM)



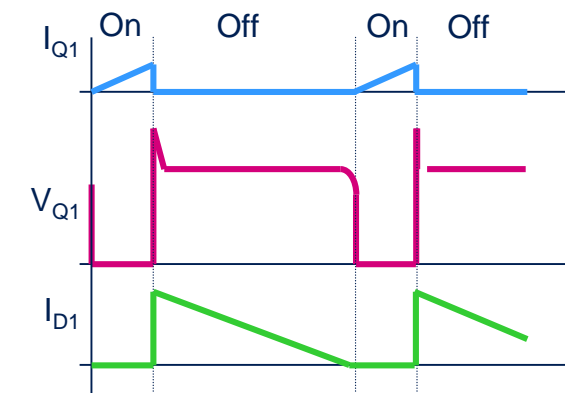
- **Benefit**
  - Higher power capability
  - Smaller transformer
  - Smaller output caps
- **Drawback**
  - Not ZCS – worse EMI and switching Losses
  - Control instability possible
- **Where to Use**
  - Higher peak power demands
  - Lower input voltages, e.g., 110V

## Discontinuous Mode (DCM)



- **Benefits**
  - ZCS turn-on of MOSFET
  - ZCS turn-off of diode
  - Simple Feedback loop
  - Low noise
  - Lower switching cap loss
- **Drawbacks**
  - EMI due to self-oscillating
  - Unused Time slot
- **Where to Use**
  - Higher input voltage, e.g., 230V

## Transition Mode (TM)



- **Benefits**
  - ZVS turn-on of MOSFET
  - ZCS turn-off of Diode
  - Simple feedback loop
  - Low noise
- **Drawback**
  - Variable frequency could be problematic for EMI
- **Where to Use**
  - When efficiency is a concern

# Select Switching Frequency

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- Three fixed frequencies:  $30\pm 3\text{kHz}$  ,  $60\pm 4\text{kHz}$  and  $115\pm 8\text{kHz}$
- Priority on transformer size?
  - Higher frequency allows to reduce  $L_p$  using less turns and smaller core size
- Priority on power efficiency?
  - Lower frequency allows to improve the efficiency

TYPICAL CORE SIZE VERSUS OPERATING FREQUENCY

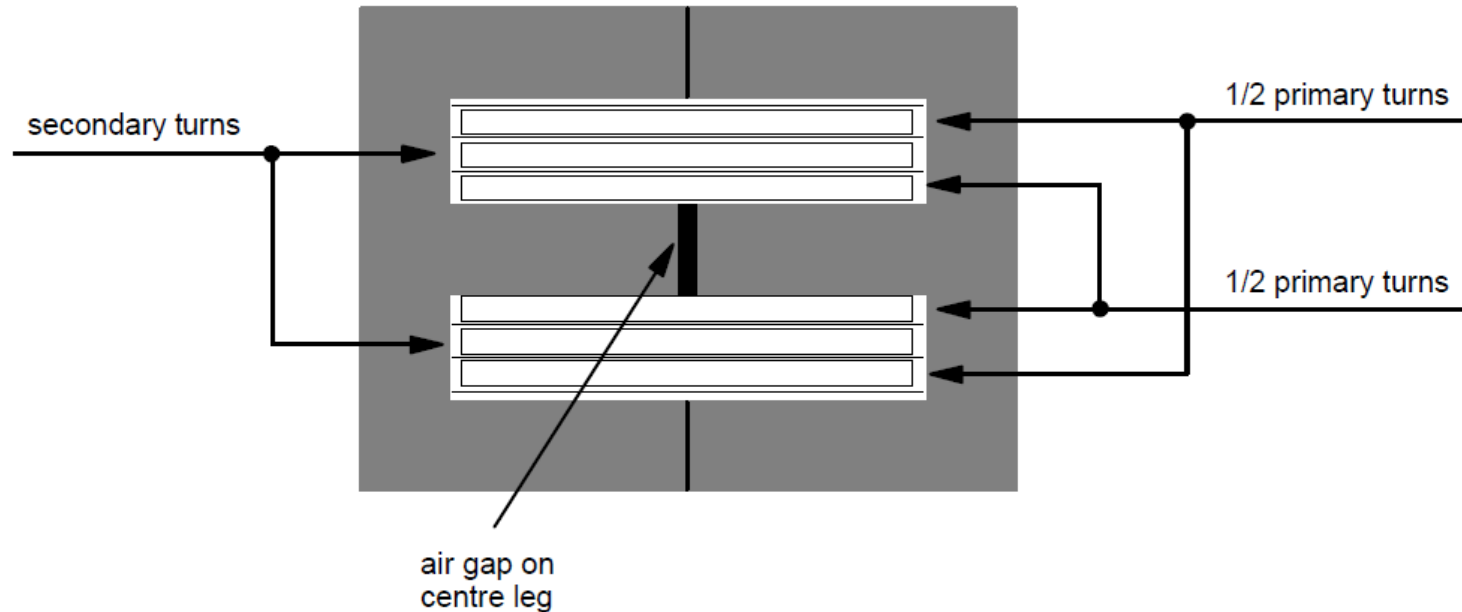
Frequency	E10	E13	E16	E20	E25
30 kHz	1.5 W	2 W	4 W	7 W	
60 kHz	3 W	4 W	6 W	13 W	25 W
115/120 kHz	5 W	6 W	8 W	18 W	32 W

- Basic specification of transformer include
  - Size, isolation barrier, reflected voltage, peak (or saturation) current, frequency, input voltage range, output voltage and output current range
- Leakage inductance influence power loss, snubber and EMI
  - Typical leakage inductance is 1~3% of primary inductance depending on the transformer structure
  - $P_{\text{Leakage}} = \frac{1}{2} L_{\text{Leakage}} I_P^2 \times f_s$
- Reflected Voltage  $V_R$  is the voltage reflected from secondary output to the primary of transformer

# Minimizing Leakage by Interleaving

12

- Leakage inductance can be reduced by splitting primary winding in 2 halves and sandwiching secondary winding in between



# Reflected Voltage Selection

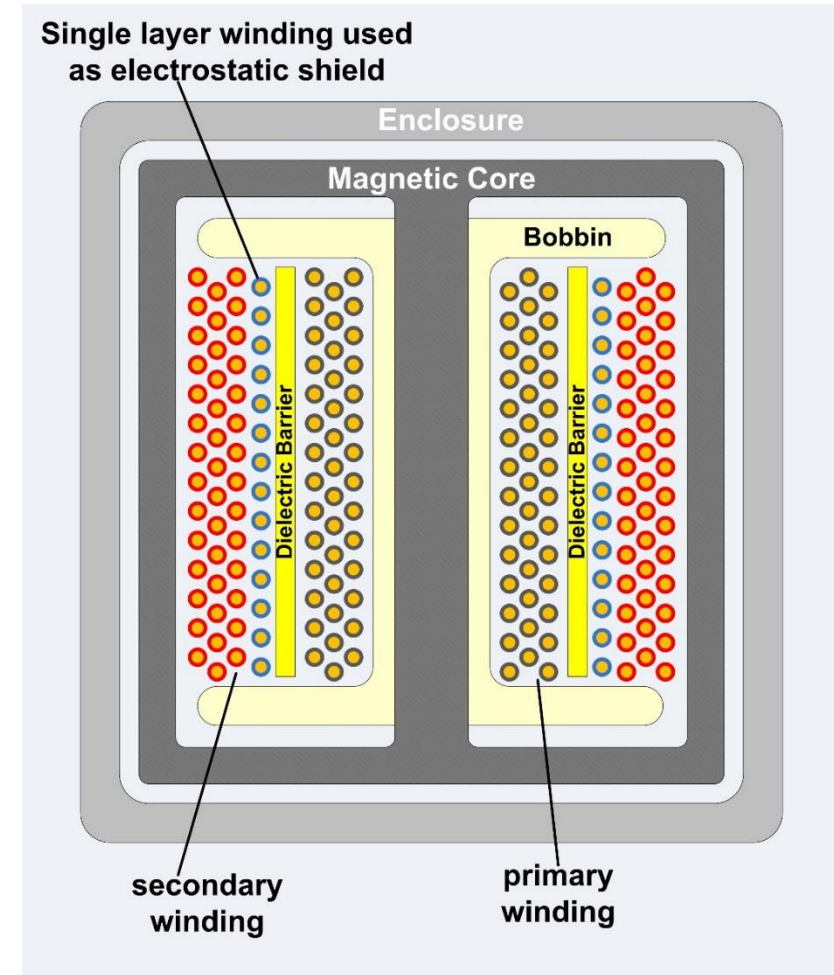
13

- Optimize reflected voltage to set maximum duty cycle. As a rule of thumb, make it equal to minimum DC input voltage
- High reflected voltage means high  $V_{ds}$  stress and higher snubber losses
- Lower reflected voltage means higher off time, higher RMS losses and higher primary peak current
- A positive side effect of lower reflected voltage is that it leads to better magnetic coupling between windings, which, in turn, helps to reduce leakage inductance

# Shielded or Non-Shielded

14

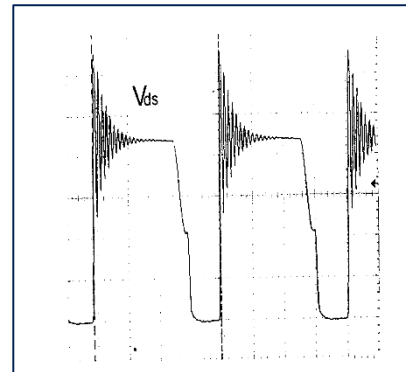
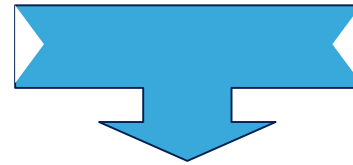
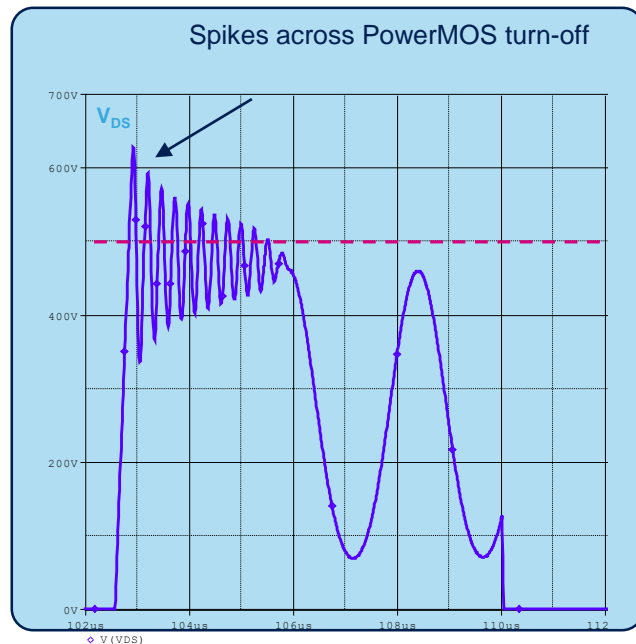
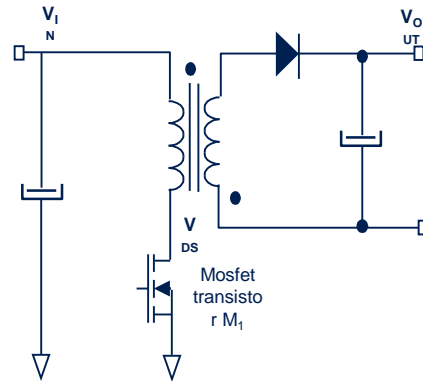
- Shielded transformer has better EMI but **larger leakage inductance**
- Non-shielded transformer has worse EMI but smaller leakage inductance



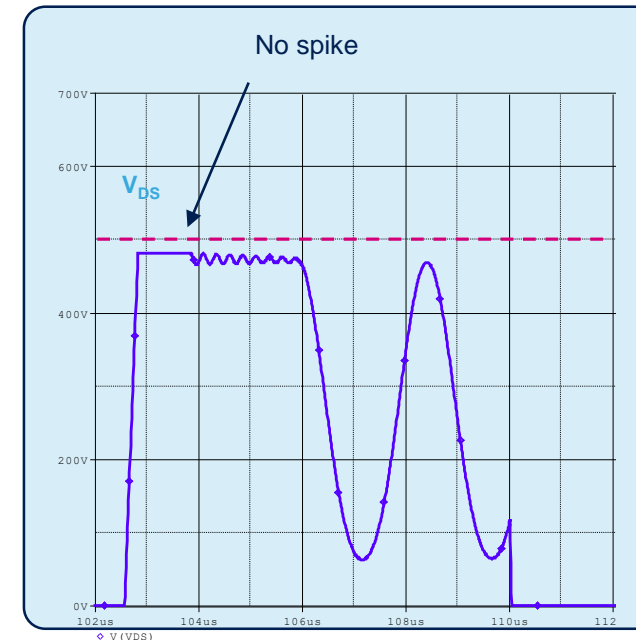
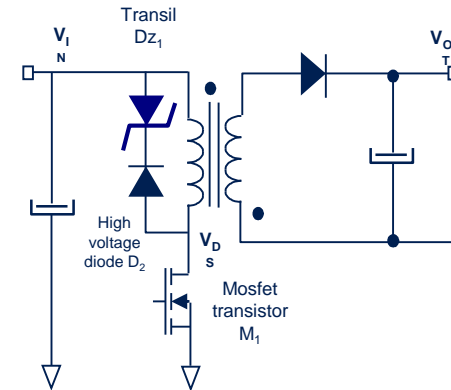
# Clamp Circuit

15

Without  
Clamp  
Circuit

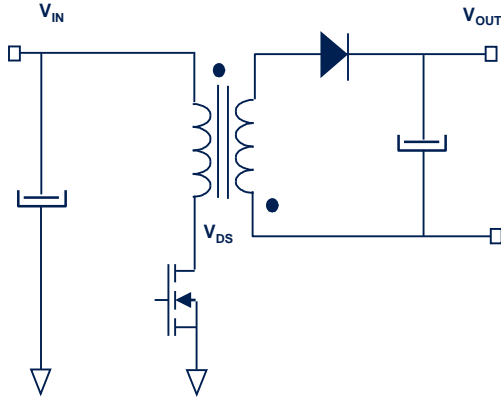


With Clamp  
Circuit

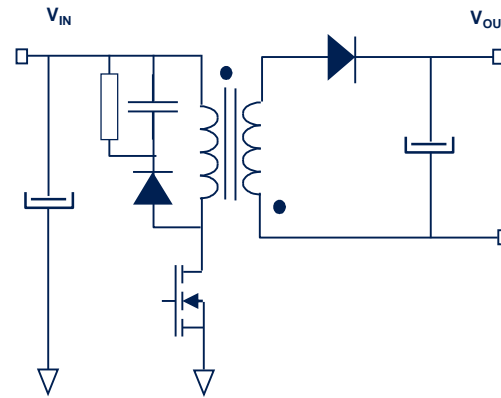


# Clamp Implementations

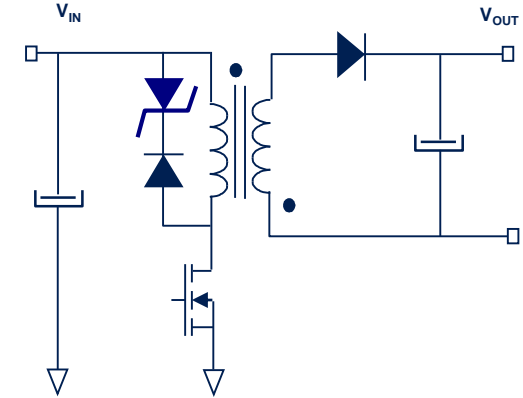
16



- No protection
- Test to be performed to know max  $V_{DS}$
- MOS / IGBT to be oversized in voltage (more expensive, efficiency drop)



- RC to limit  $dV/dt$ , then to limit overvoltage
- Slope may vary depending on components
- Margin on  $V_{DS}$  is depending on components
- Test to be done for validation

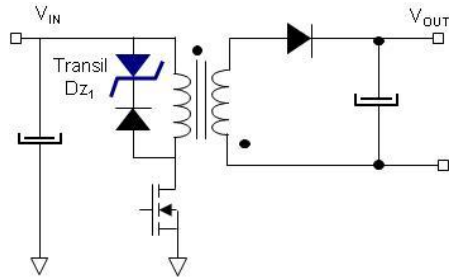


- Maximum clamping voltage only depends on STRVS
- Datasheet/product adapted to repetitive surges
- Margin on  $V_{DS}$  can be easily calculated
- Validate with minimal test

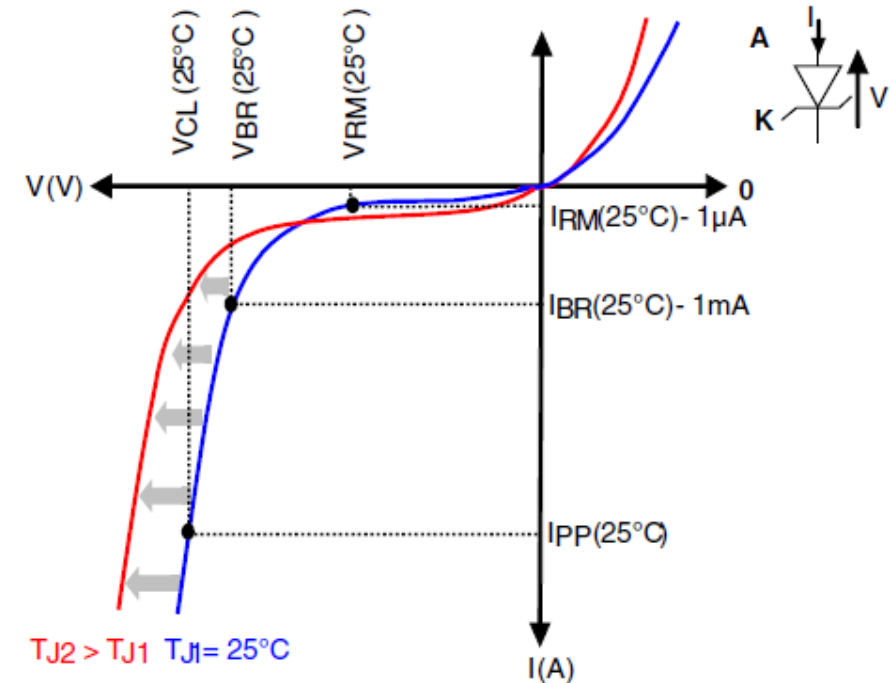


# New Clamping Technology: STRVS

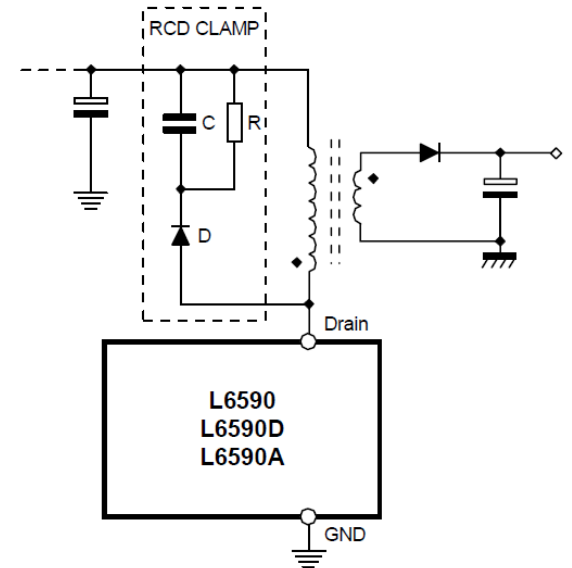
17



- VRM is stand-off voltage and must be selected to allow the FET to switch:  $VRM > VR$
- VCL is the clamping voltage and is critical to choose as close as possible to the application requirement
- Extensive data published on STRVS datasheet makes the selection for the right part easy and robust



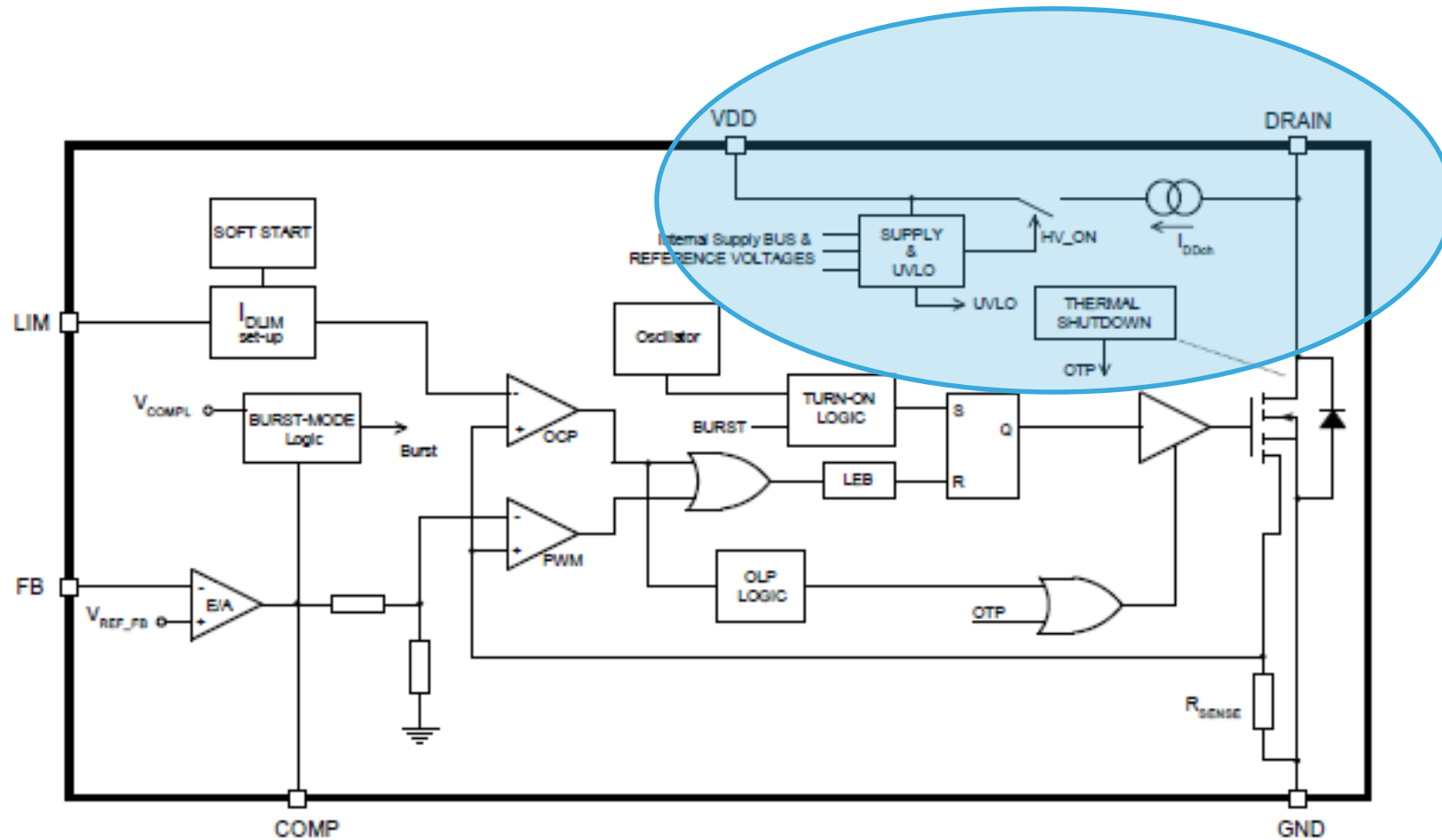
- RCD sizes and values need to be carefully selected. There is a tradeoff between RC values, power dissipation, EMI and clamping effect
- RCD clamp dissipates power even under no-load conditions: there is always the reflected voltage across the clamp resistor R



R	C	$V_{CL}$	$V_{DS}(PK)$	EMI	$P_{DISS}(R)$	Cost
↓	↑	↓	↓	↓	↑	↑
↑	↓	↑	↑	↑	↓	↓

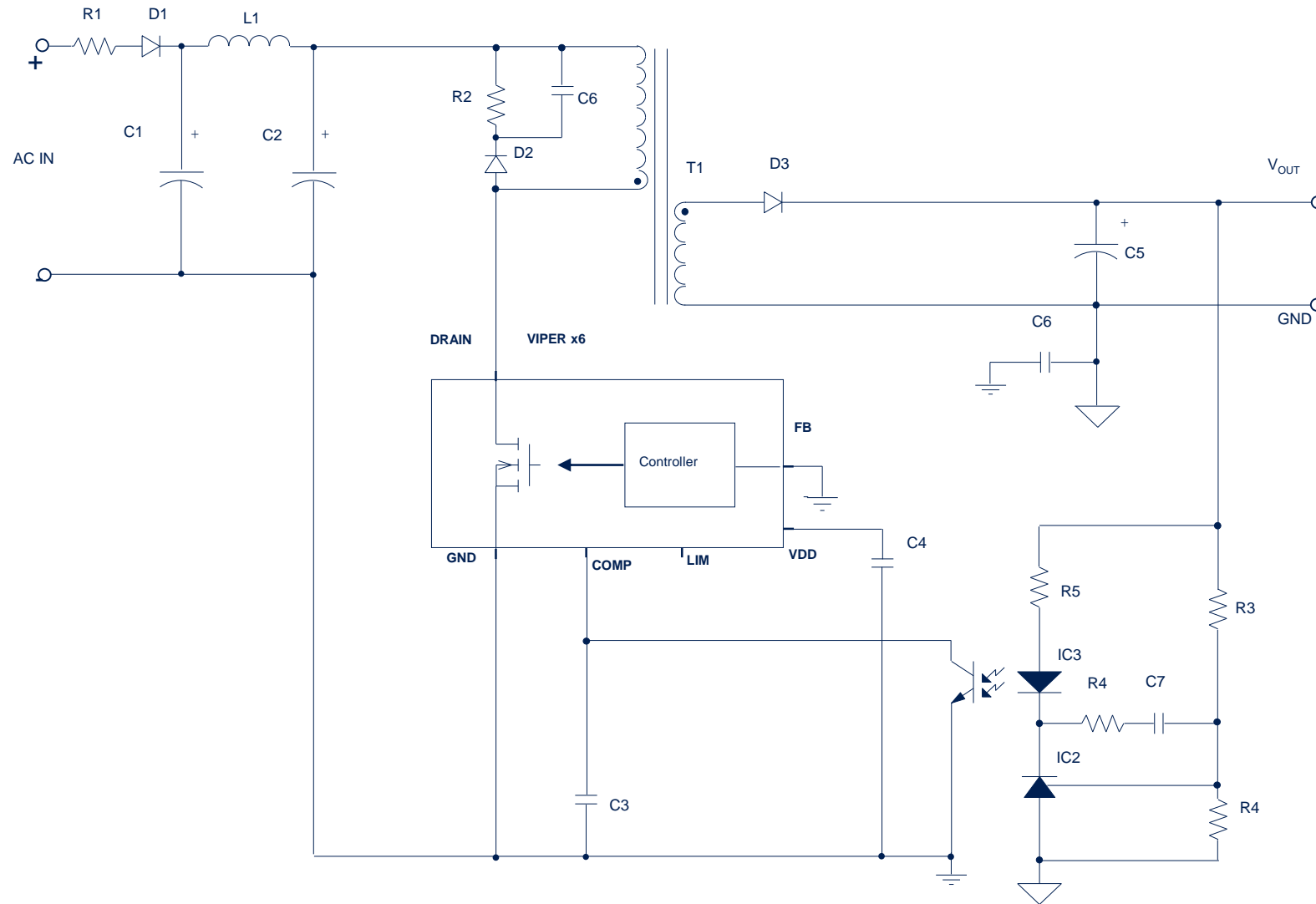
# Stand-By Consumption: HV Start-Up

19



# Stand-By Consumption

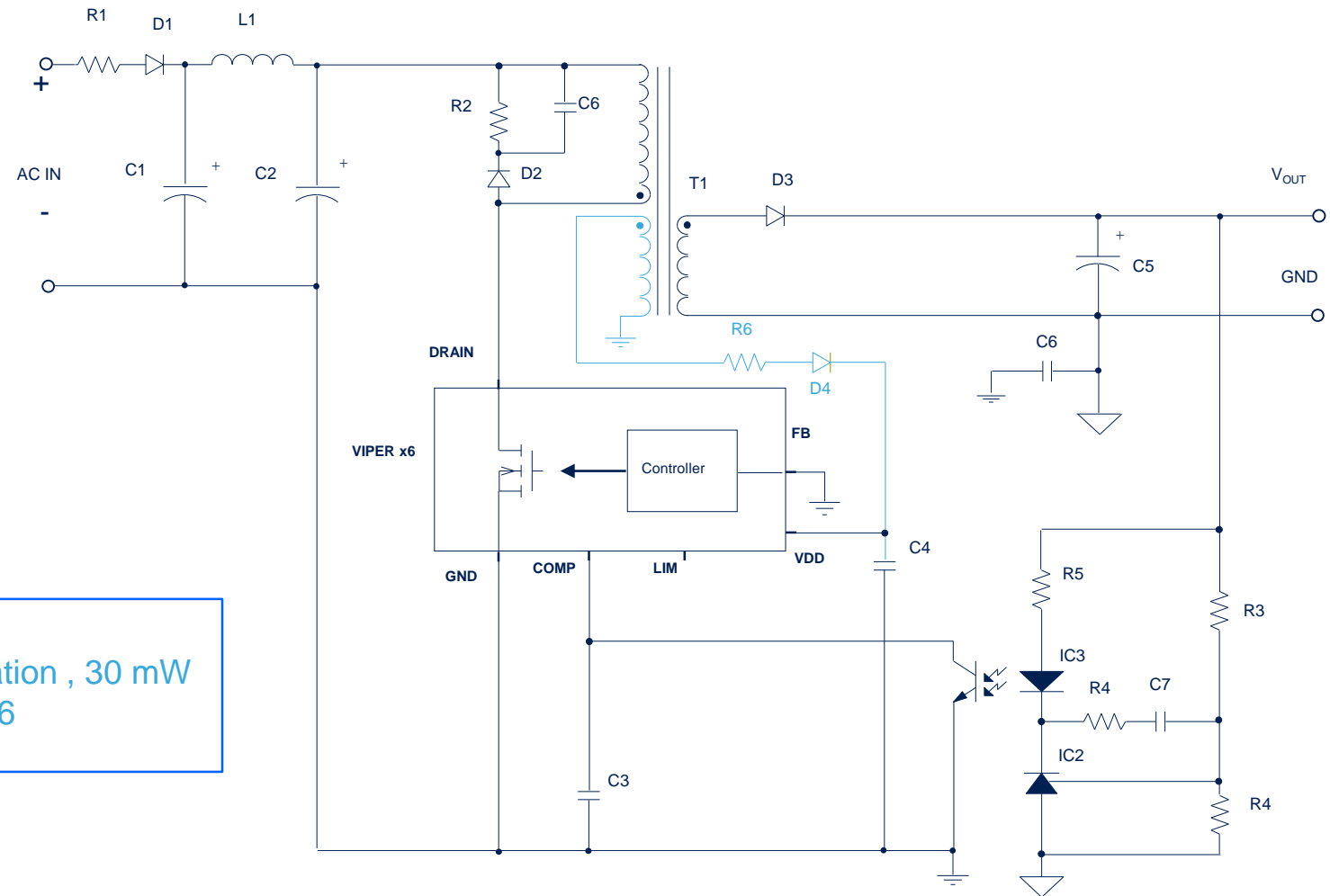
20



# Stand-By Consumption

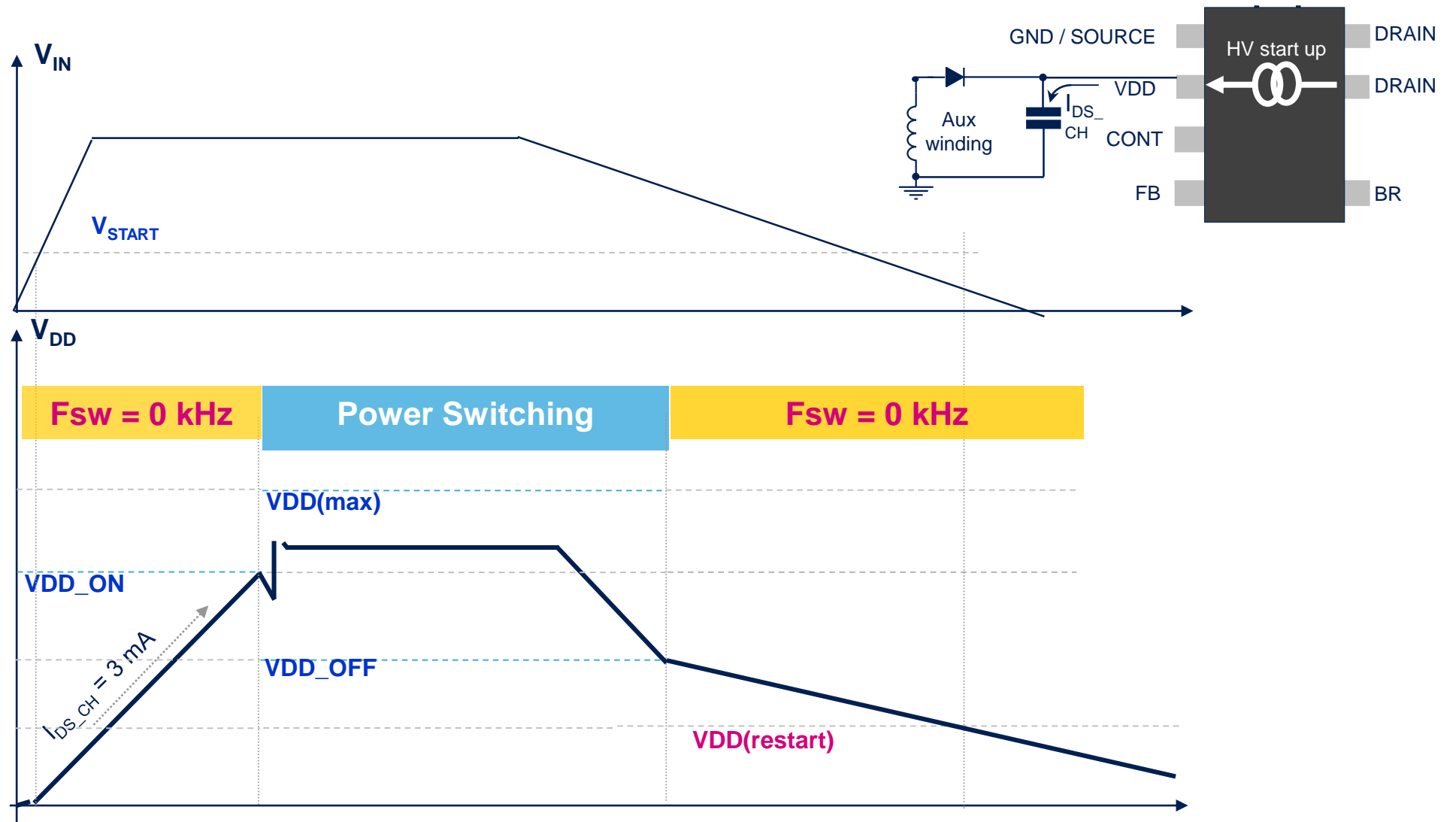
21

Stand-by optimization , 30 mW  
D4, R6



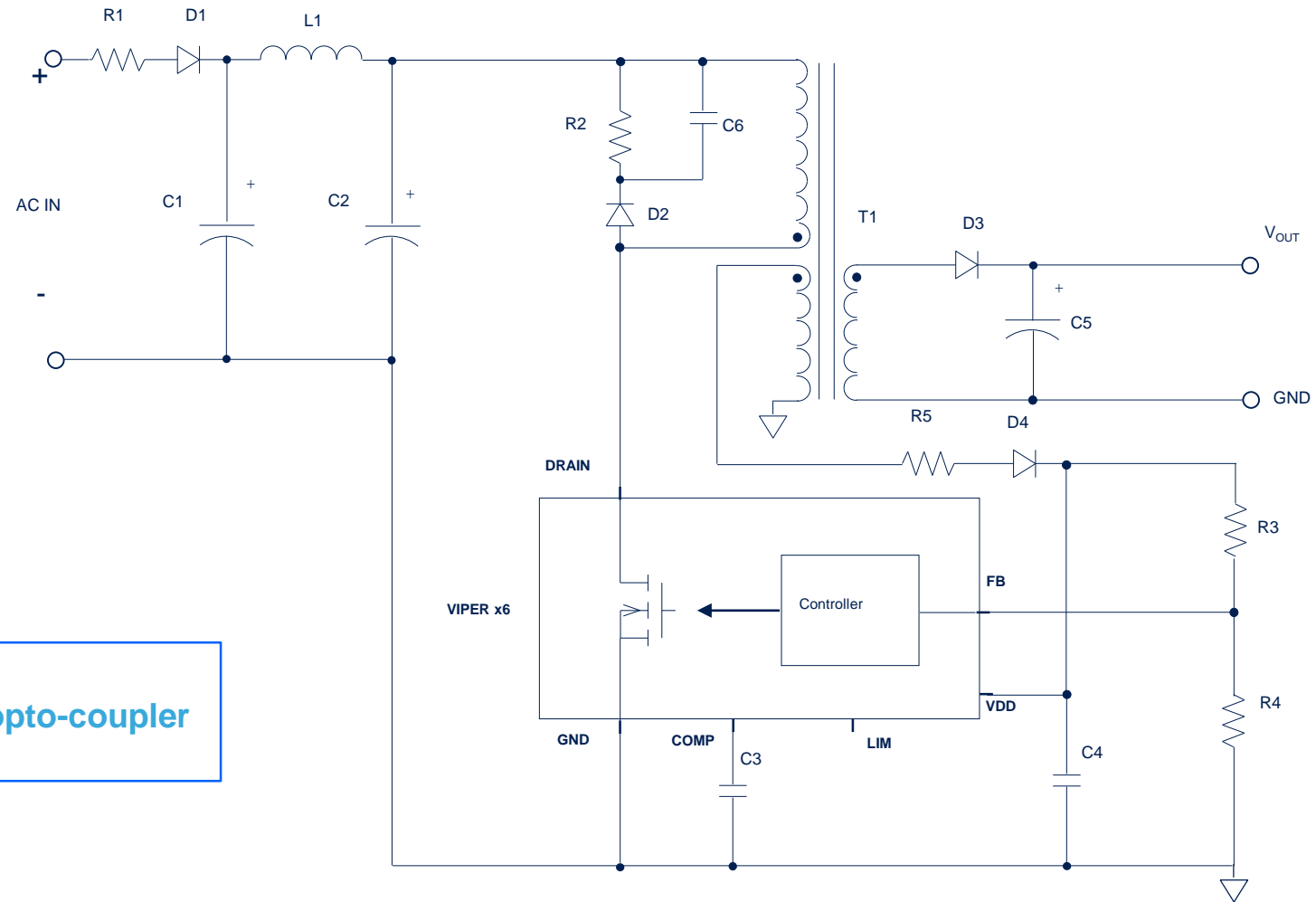
# Stand-By Consumption: HV Start-Up

22



# Stand-By Consumption

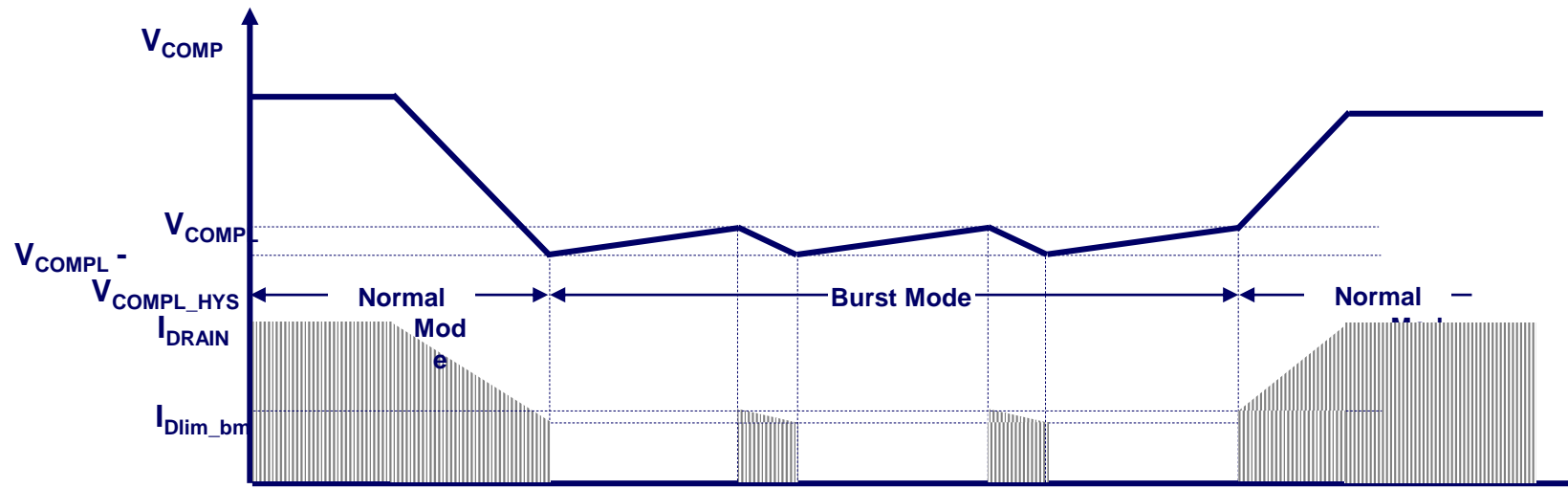
23



No need of the opto-coupler

# Stand-By Consumption: Burst Mode

24



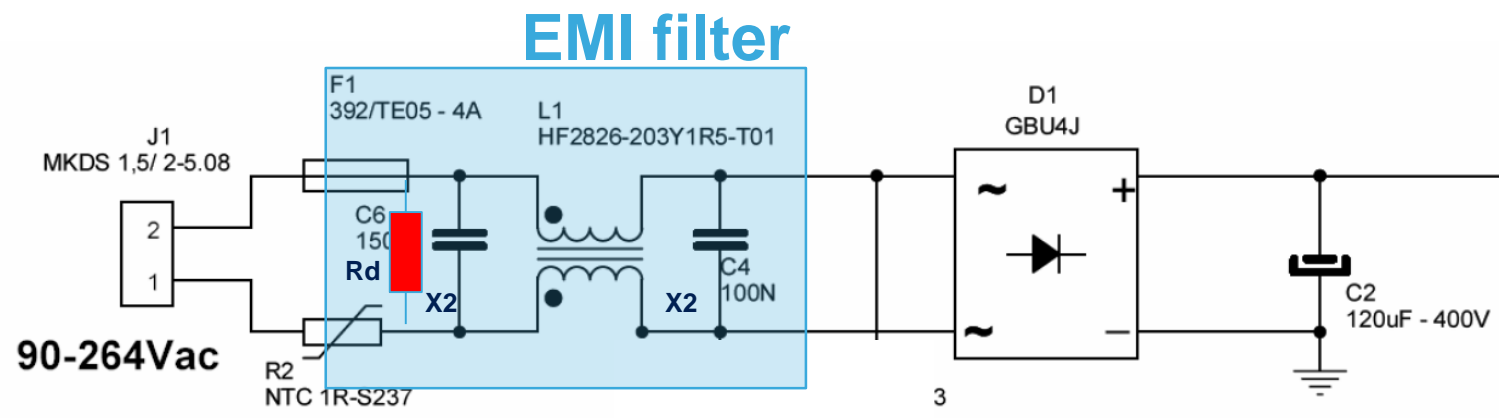
$V_{COMP} < V_{COMPL}$  starts burst mode



# X-Cap Discharge

25

- The EMI filter in the input of the power converter typically consists of capacitors across the AC mains and CM choke
- According to safety regulations, e.g. UL 1950 and IEC61010-1, capacitors on the mains must be discharged within a given time after the appliances is suddenly disconnected
- A discharge resistor is typically connected in parallel, resulting in additional power losses, as long as the appliance is plugged
- A new function has been recently introduced in order to actively discharge the X capacitor through the HV start-up circuit

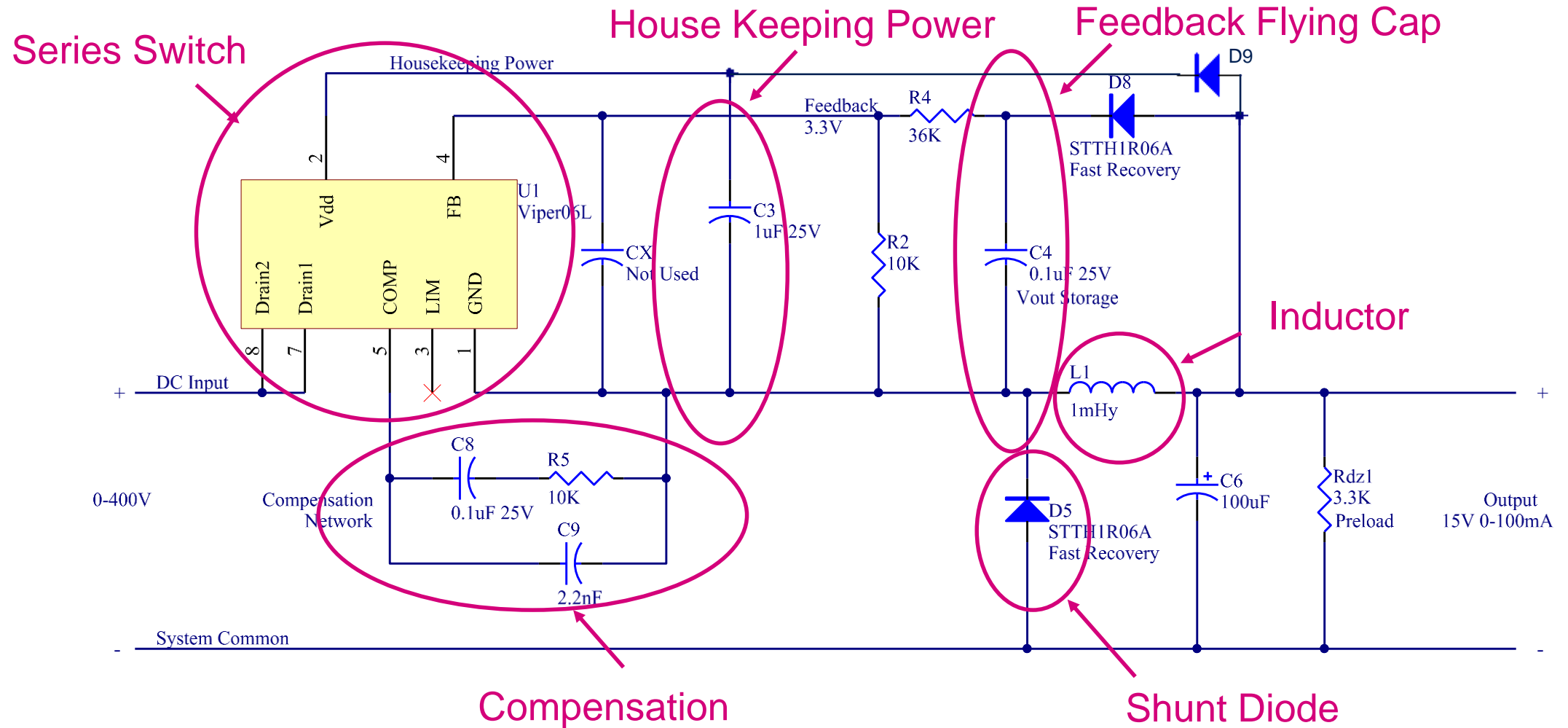




# Buck Topology Optimization

# Buck Schematic

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# “Flying Capacitor” Feedback Scheme

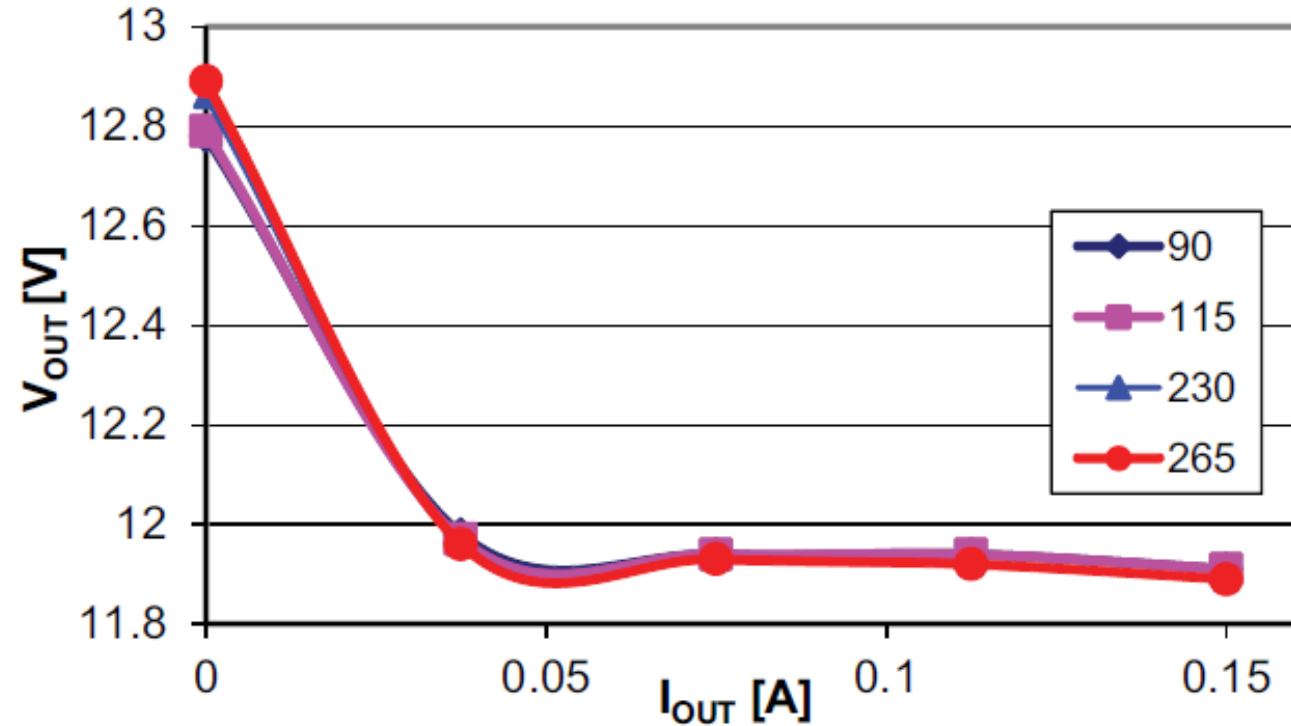
28

- C4 stores output voltage, transfers level into Viper feedback loop
- R4 – R2 discharge C4 slowly
- Load current is required to turn on D5 and D8 to charge C4
- A light load MUST be present to ensure diode turn-on
- C4 must hold output voltage information when Viper is in burst mode

# “Flying Capacitor” Feedback Scheme (Cont.)

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- Low cost solution
- Minimum load required



# Select Switching Frequency

30

## SELECT FREQUENCY FOR 5 V OUTPUT BUCK

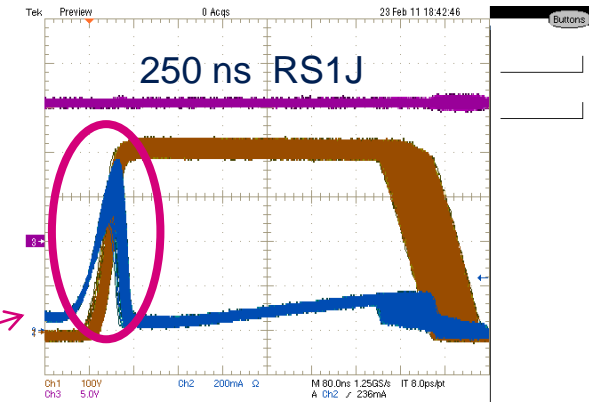
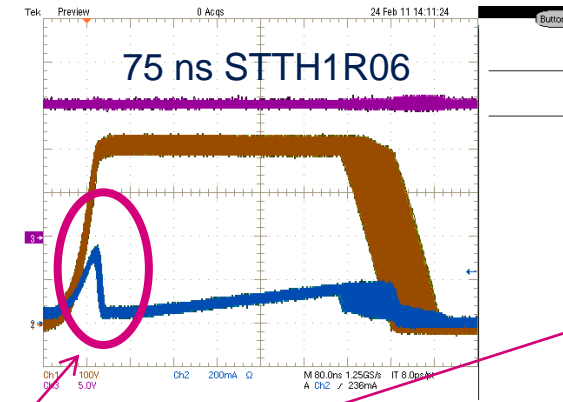
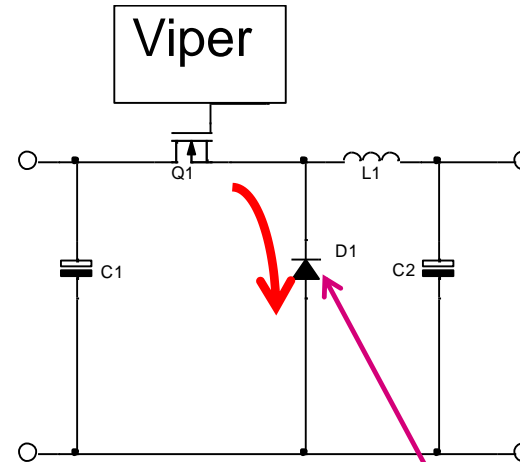
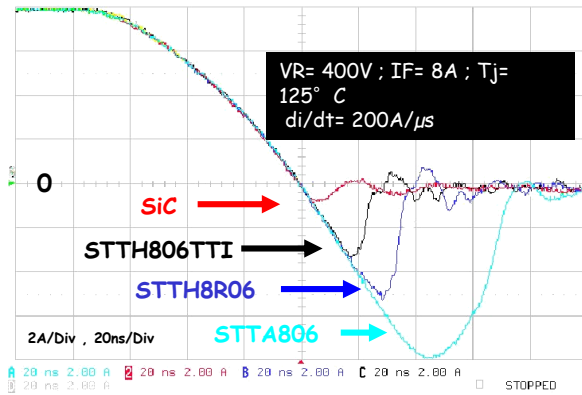
Vin DC (V)	D (%) 5 V	t <sub>ON</sub> (μs) for 60 kHz 5 V	t <sub>ON</sub> (μs) for 30 kHz 5 V	VIPer01 Minimum ON time
100 (85 VAC)	5.0	0.83	1.67	0.35 μs
170V (120 VAC)	2.9	0.49	0.97	
325V (230 VAC)	1.5	0.26	0.50	
375V (265 VAC)	1.3	0.22	0.33	
622V (440 VAC)	0.8	0.13	0.26	

Lower frequency allows to handle the regulation even in the case of a very high ratio between input and output voltages

- Duty cycle of Viper Buck converter is limited by minimum on time
  - Viper06 450 ns
  - Viper01 350 ns
- If the required ON time is shorter than minimum ON time, Buck still works, but there is small instability and the maximum deliverable output current is reduced.
- The 30kHz version is strictly recommended for 5V output

# Diode Recovery Effect

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Recovery effect causes short cross conduction every turn ON. Effect is much critical in case CCM => **DCM is recommended**. The lost energy is higher at higher power operating frequency => **The 30kHz version is recommended**.





# Layout and EMI Optimization

- Minimize **interconnection lengths** of following components:
  - Input filter caps, input-side transformer (or inductor), power MOSFET, sensing resistors and active-clamp or **snubber circuits**
  - Output-side transformer (or inductor), rectifier diodes and **output filter caps**
- Keep **power and signal circuitries separated** and be careful of connection between the signal and power grounds
- Assure component isolation and **spacing by safety standards**
- **Prioritize ground** over all routes
- **Large copper areas** for thermal and EMI
- Add **sufficient VIAs** for better thermal performance
- Keep the **feedback path** as far as possible from power components and noise traces
- External **compensation components** should be **close to IC**
- Copper **traces for power** should be **thick and short** and **sharp angles** should be avoided

- EN 55022 is an European EMC standard applicable to information technology equipment with a rated supply voltage not exceeding 600 V
- Properly size EMI filter: differential mode filter for power < 5 W; X-, Y-caps, and common mode choke for power > 15 W
- Designers often use snubbers and soft switching techniques to minimize the EMI
- Shielded transformer has better EMI but also has larger leakage inductance
- Connect heatsinks to ground
- Focus on coupling paths from EMI sources to EMI sensitive components
- Strategic orientation and placement of components can reduce EMI generation significantly
- Eliminate environmental interference on EMI test
- Use an accurate EMI analyzer to carry quasi-peak, and average measurement to meet standards
- ST offers PWM operation with frequency jittering for low EMI





# EDesignSuite Examples

<https://my.st.com/analogsimulator/>  
Create an ST.com account and  
use it to sign in to eDesign Suite

Dashboard

Converter

Battery Charger

LED Driver

Photovoltaic

Signal Conditioning

RF Design

AC Control

Smart Selectors

Configurators

Help

# eDesignSuite

## The smart design tool



life.augmented

eDesignSuite

Dashboard

Converter

Battery Charger

LED Driver

Photovoltaic

Signal Conditioning

RF Design

AC Control

Smart Selectors

Configurators

My projects

Examples

life.augmented

eDesignSuite

Dashboard

Converter

AC/DC

PFC Pre-regulation

PWM Controllers

Non isolated

Isolated

Examples

Name

Battery charger

LED Driver

Photovoltaic

Power Supply

AC/DC

Non isolated

Buck

FF Flyback

My projects

Examples

life.augmented

eDesignSuite

Dashboard

AC/DC

Isolated

FF Flyback

QR Flyback

Examples

Name

Battery charger

LED Driver

Photovoltaic

Power Supply

Previous Version

Refresh

Import

?

Help

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eDesignSuite

Previous Version



40

Converter > AC/DC > Non isolated > Buck

Collections

Features

Search



22 Results

Number of products available

Topology

Can search by part number

Specifications

Reset All

Input

Voltage  
USA Range - 60 Hz

Min V

85

Max V

140

☐ 50 Hz ☒ 60 Hz

Output

Voltage

12

Current

0.2

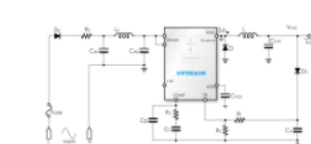
ADD OUTPUT

Output Power 2.4 W

VIPER06HN

DIP 7

Buck



IDlim: 320 mA

VBVDSS: 800 V

RDSon: 30  $\Omega$

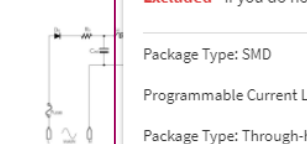
fosc: 115 kHz



START DESIGN

VIPER06HS

Buck



IDlim: 320 mA

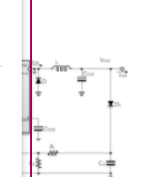
VBVDSS: 800 V

RDSon: 30  $\Omega$

fosc: 115 kHz



DIP 7



IDlim: 320 mA

VBVDSS: 800 V

RDSon: 30  $\Omega$

fosc: 115 kHz

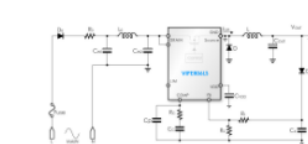


START DESIGN

VIPER06LS

SS010

Buck



IDlim: 320 mA

VBVDSS: 800 V

RDSon: 30  $\Omega$

fosc: 60 kHz

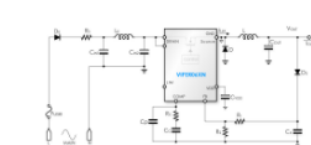


START DESIGN

VIPER06XN

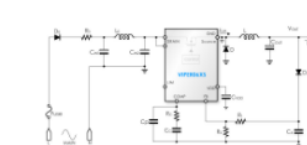
DIP 7

Buck

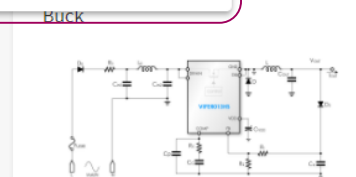


VIPER06XS

Buck



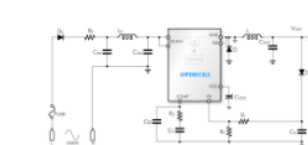
SS010



VIPER013LS

SS010

Buck



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Choose by features

Specification – input voltage range  
Output voltage/current



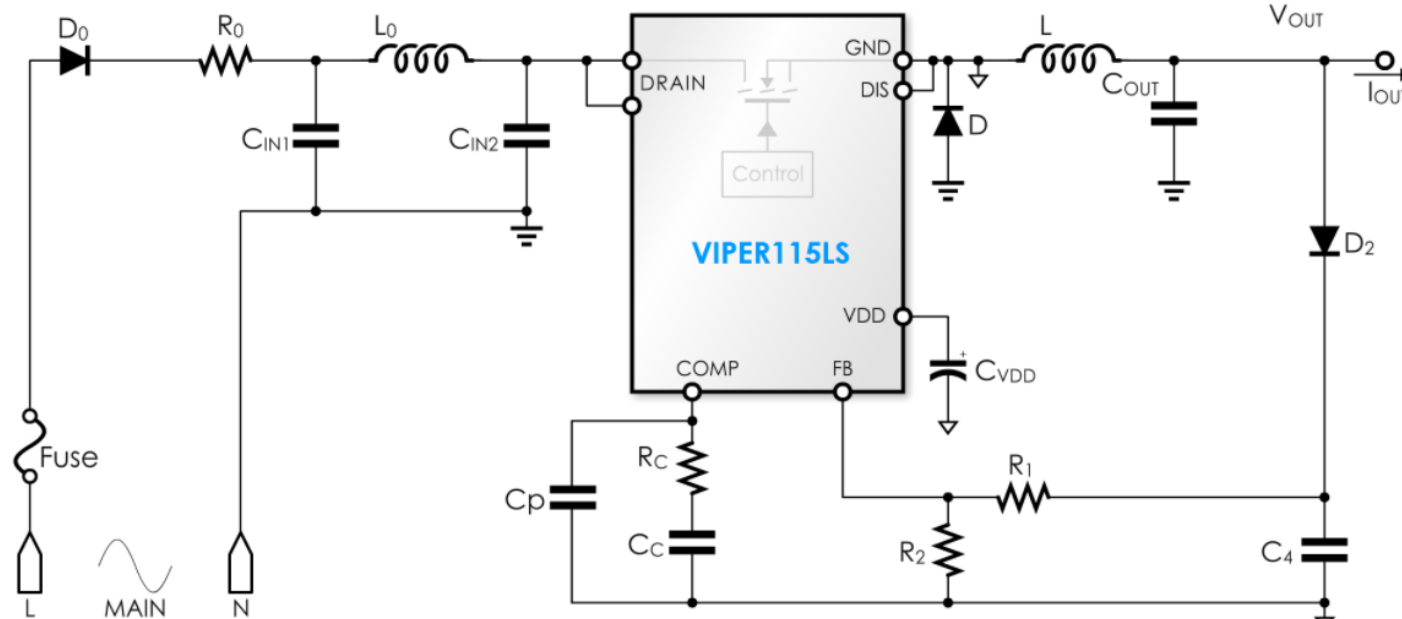
life.augmented




**VIPER115LS**

SS010

Buck


**Specifications**

Reset All

**Input**

Voltage  
USA Range - 60 Hz

Min V

85

Max V

140

50 Hz 60 Hz

**Output**

Voltage

12

Current

0.2

Output Power 2.4 W

Selected device, design specification and generic schematic  
– once all that is ready proceed with **START DESIGN** button

**START DESIGN**

IDlim: 575 mA

VBVDSS: 800 V

RDSon: 17 Ω

fsw: 60 kHz

Datasheet

Product Folder

Energy saving off-line high voltage converter

Main features:

- 800 V avalanche-rugged power MOSFET allowing ultra wide range input VAC to be achieved.
- Embedded UV protection and zero VDS

**eDesignSuite**

**Design commands**

Redesign Save Print Disclaimer

Help Size

**Converter Specifications**

IC: VIPER115LS - SSOT10  
 Input: 85 Vac - 140 Vac - 60 Hz  
 Output Power: 2.4 W  
 Out 1: 12 V (2 % ripple) - 200 mA max

[Change Specifications...](#)

**Actuals @ VinAC: 140 V**  
 Iout: 200 mA  
 Ta: 25 °C

Vout: 12.01 V ripple: 157 mV - 1.3%  
 IL ripple: 475 mA  
 fsw: 60 kHz Ton: 935.4 ns  
 bandwidth: 0.76 kHz  
 phase margin: 77.01°  
 average Vin DC: 179.9 V  
 input currents  
 avg: 15 mA peak: 188 mA rms: 63 mA  
 burst mode: no conduction mode: DCM  
 ΔTj: 21 °C IC Tj: 46 °C

[Design refinements...](#)

**Circuit**

Schematic BOM

**Toolbox icon lets you adjust parameters**

**Bill of materials and schematic**

**Annotated and interactive schematic**

**The user can customize some of the characteristics**

**Operating conditions can be varied**

**Specification**

**A set of qualitative metrics**

**Click to maximize**

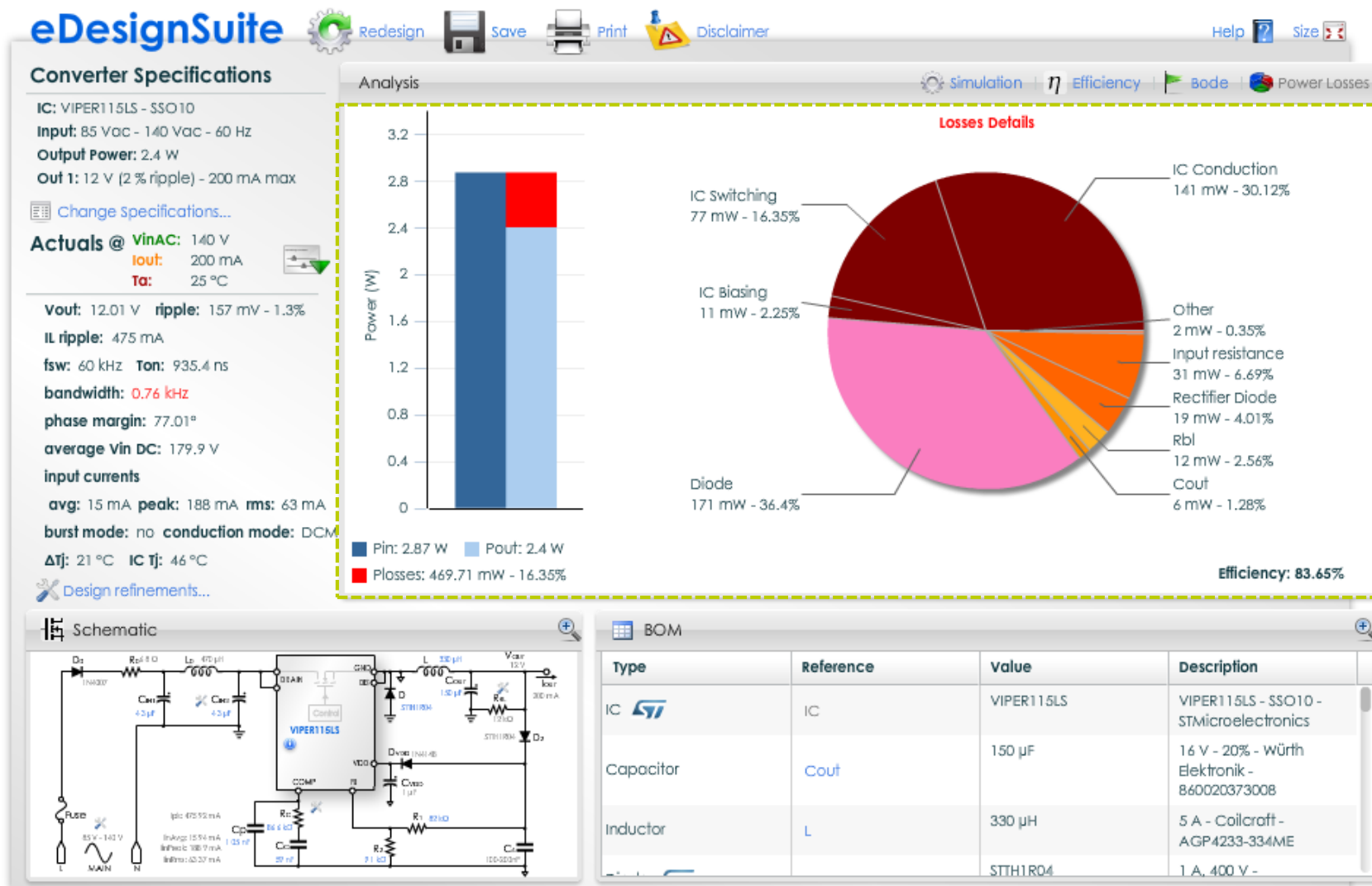
Simulation: duty cycle 5.6%

η Efficiency: 83.6 %

Bode: fc = 755.51 Hz - phase margin = 77 °

Losses: 469.7 mW - 16.4%

IC: 229 mW - 48.72%  
 Diode: 171 mW - 36.4%  
 Input losses: 50 mW - 10.69%  
 Rbl: 12 mW - 2.56%  
 Cout: 6 mW - 1.28%  
 Other: 2 mW - 0.35%



Very useful losses distribution chart



Thank You!