

AC-DC SMPS: Up to 15W Application Solutions

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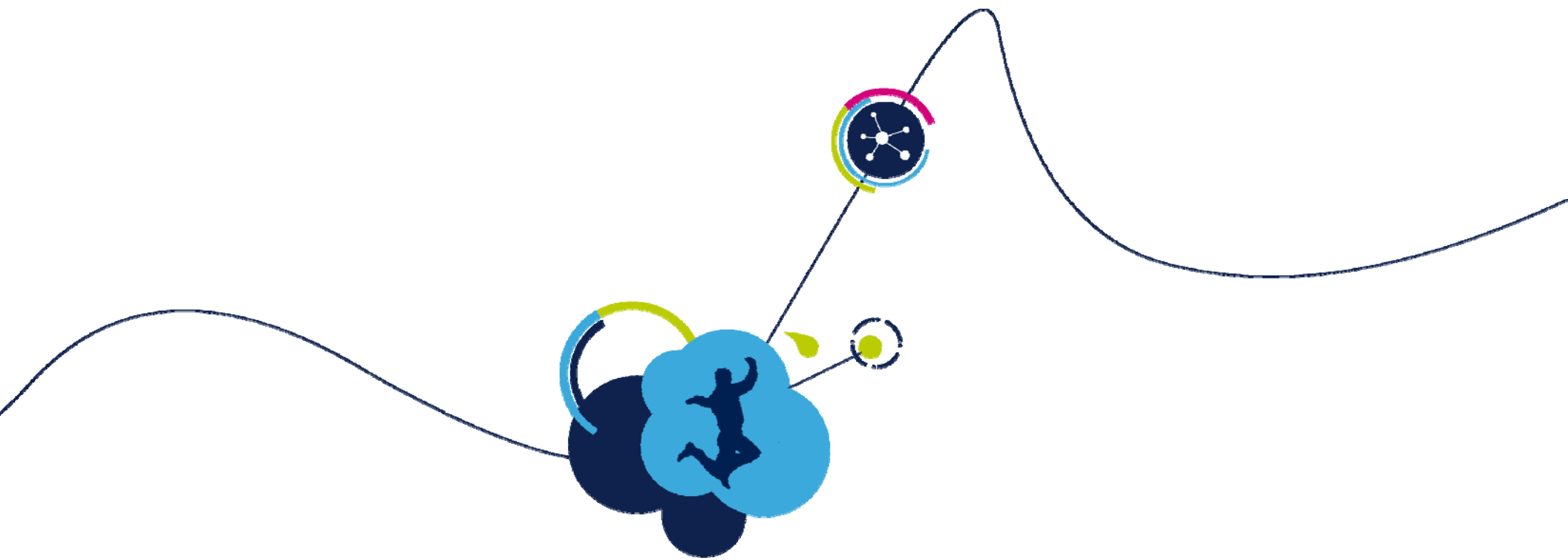


Technology
Tour 2017



Agenda 2

- Introduction
- Flyback Topology Optimization
- Buck Topology Optimization
- Layout and EMI Optimization
- eDesignSuite Examples



Introduction

Applications

4

Auxiliary Power Supply

Major Appliances



Air conditioning



Industrials



Lighting



Electrical Vehicle



Main Power Supply

Smart Meters



Smart Buildings



Small Industrials



Small Appliances

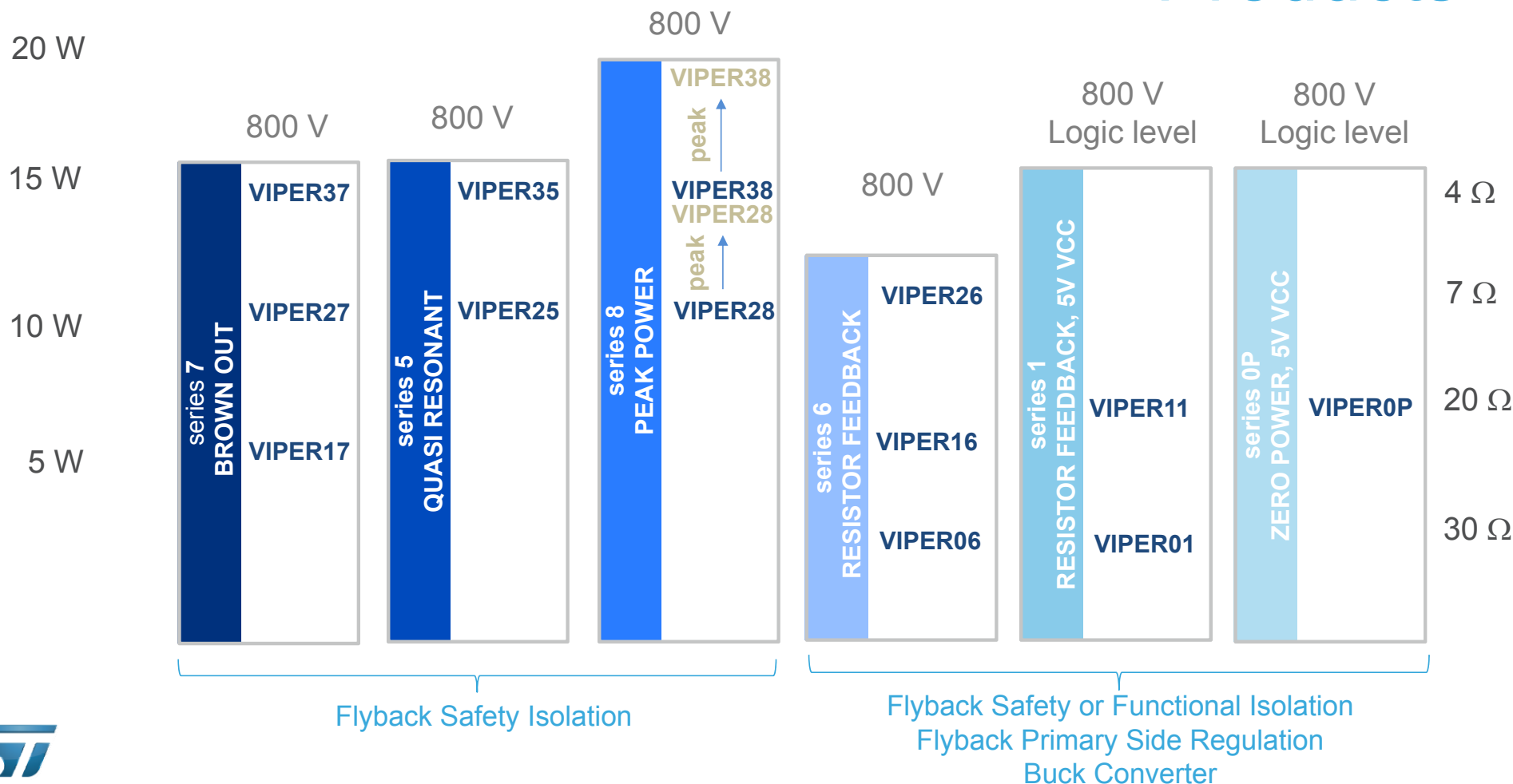


Adapters



Products

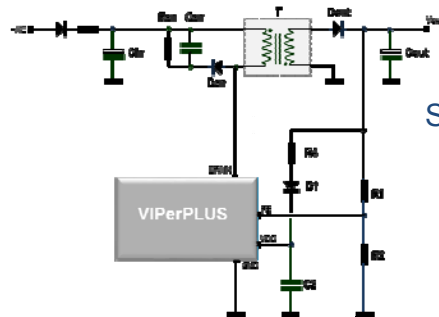
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Which Topology?

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Functional Isolation



Secondary Regulation
with Resistor Divider

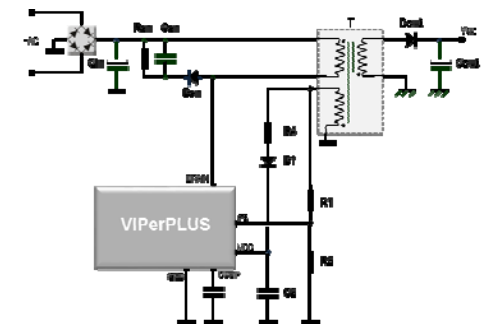
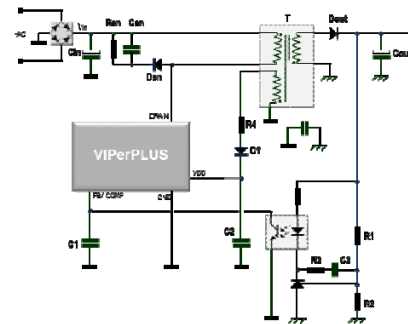
Flyback
Converter



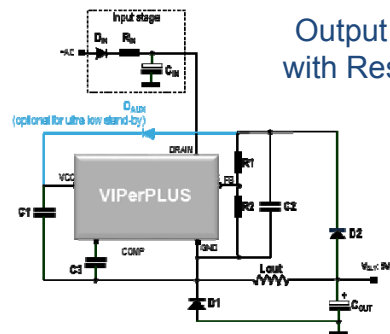
Galvanic Isolation For Touchable Outputs

Secondary-Side Regulation
With Opto-Coupler For Tight Regulation

Primary-Side Regulation
Without Opto-Coupler



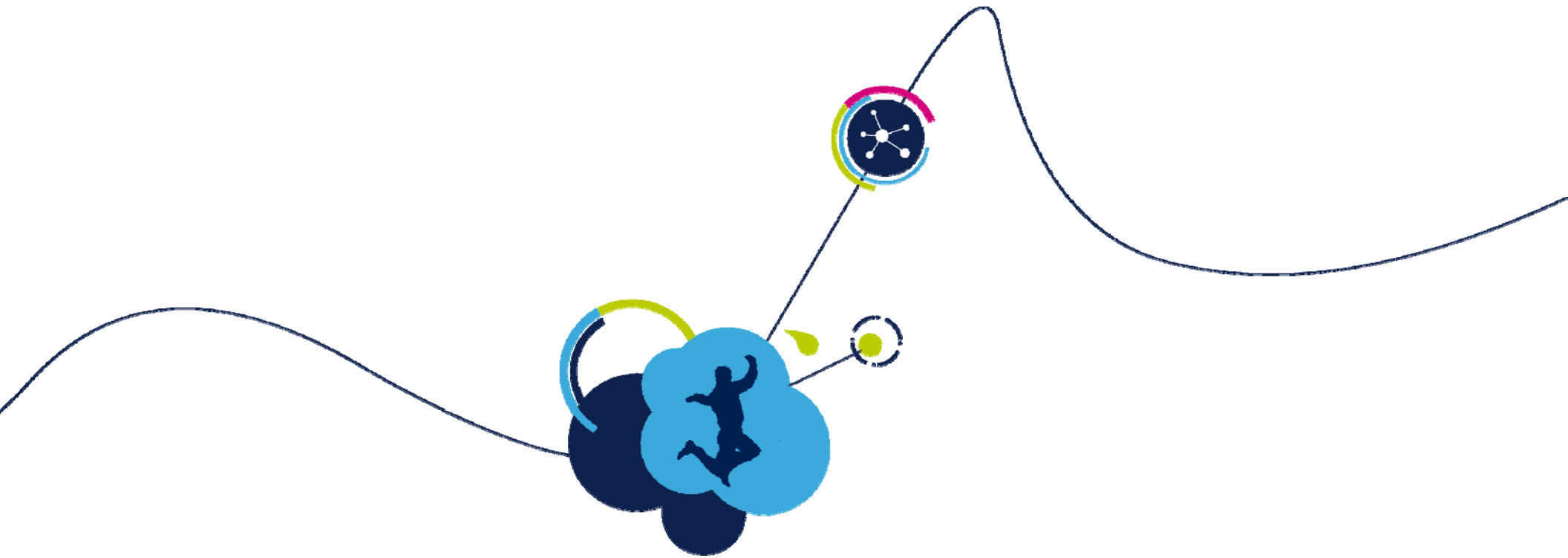
Buck Non-Isolated



Output Regulation
with Resistor Divider

Buck Converter
Small Inductor
Compact PCB

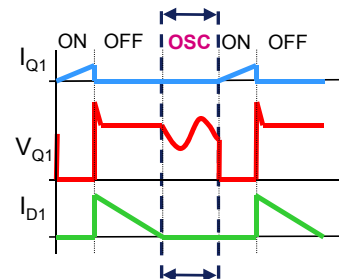
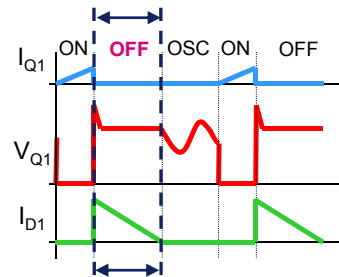
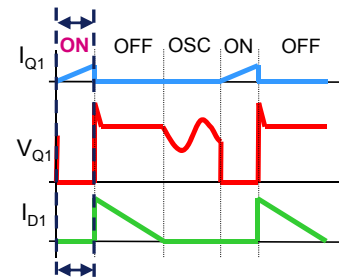
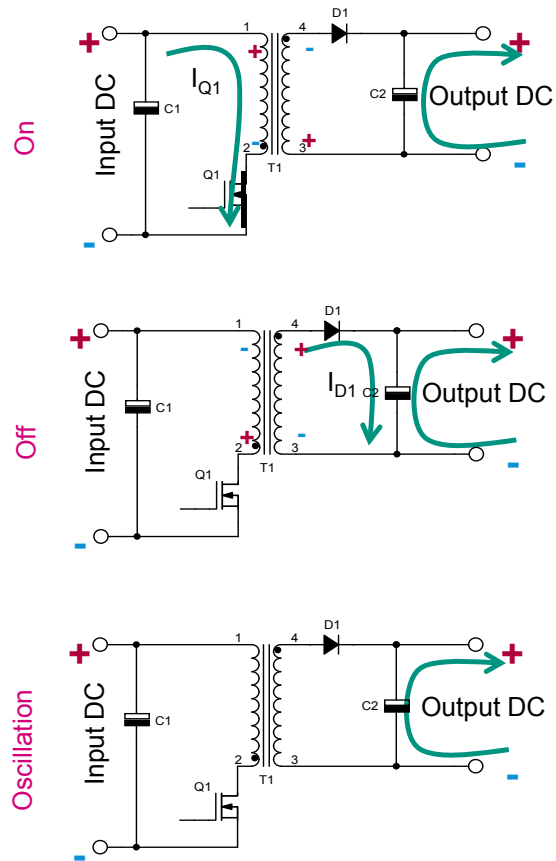




Flyback Topology Optimization

Flyback Operation

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$$E_{T1} = \frac{1}{2} L_P I_{Q1PK}^2$$

$$P_{T1} = \frac{1}{2} L_P I_{Q1PK}^2 f_{SW}$$

$$I_{D1PK} = \frac{N_P}{N_S} I_{Q1PK} = n_{T1} I_{Q1PK}$$

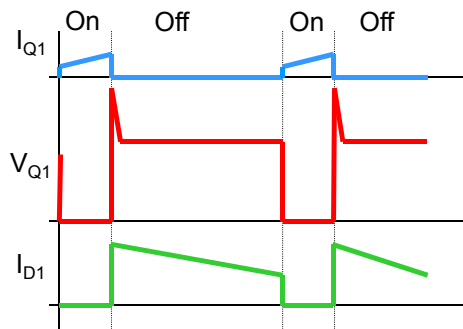
$$E_{T1} = \frac{1}{2} L_S I_{D1PK}^2$$

$$L_S = \frac{L_P}{n_{T1}^2}$$

Operation Modes

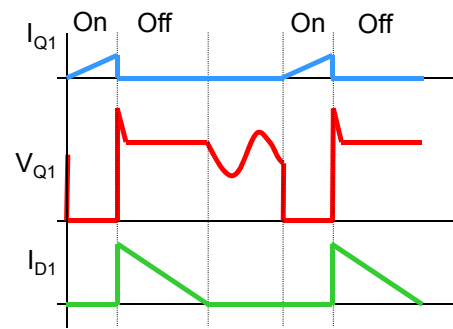
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Continuous Mode (CCM)



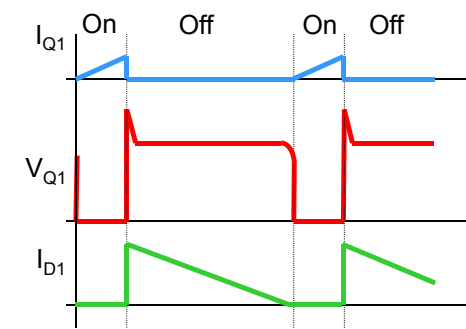
- **Benefit**
 - Higher power capability
 - Lower conduction loss
 - Smaller transformer
 - Smaller output caps
- **Drawback**
 - Not ZCS – worse EMI and switching Losses
 - Control instability possible
- **Where to Use**
 - Higher peak power demands
 - Lower input voltages, e.g., 110V

Discontinuous Mode (DCM)



- **Benefits**
 - ZCS turn-on of MOSFET
 - ZCS turn-off of diode
 - Single Feedback loop
 - Low noise
 - Lower switching cap loss
- **Drawbacks**
 - EMI due to self-oscillating
 - Unused Time slot
- **Where to Use**
 - Higher input voltage, e.g., 230V

Transition Mode (TM)



- **Benefits**
 - ZCS turn-on of MOSFET
 - ZCS turn-off of Diode
 - Simple feedback loop
 - Low noise
- **Drawback**
 - Variable frequency could be problematic
- **Where to Use**
 - When efficiency is a concern

Select Switching Frequency

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- Three fixed frequencies: $30 \pm 3 \text{ kHz}$, $60 \pm 4 \text{ kHz}$ and $115 \pm 8 \text{ kHz}$
- Priority on transformer size?
 - Higher frequency allows to reduce L_p using less turns and smaller core size
- Priority on power efficiency?
 - Lower frequency allows to improve the efficiency

TYPICAL CORE SIZE VERSUS OPERATING FREQUENCY

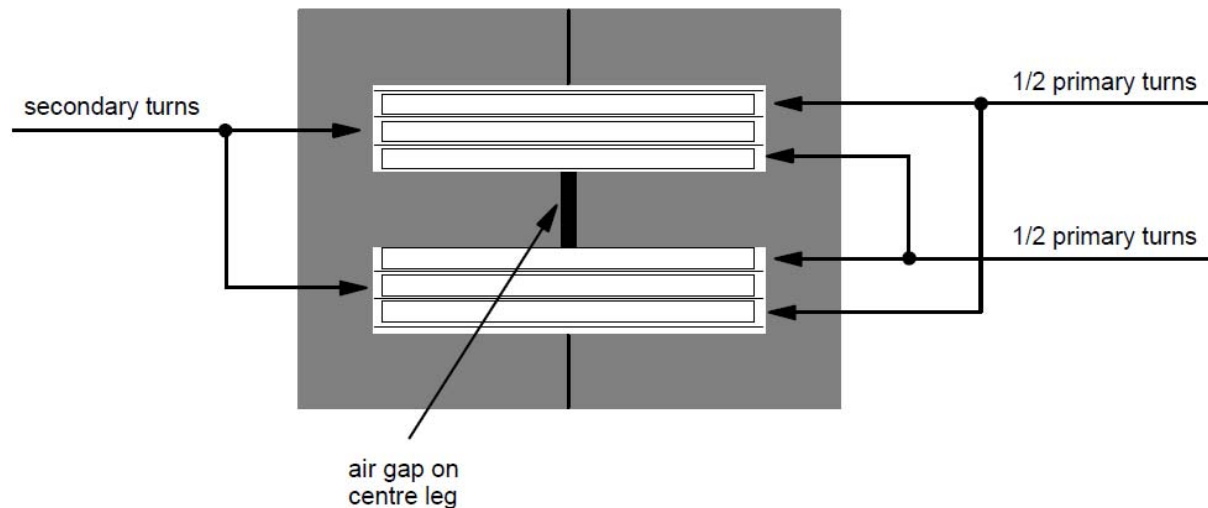
| Frequency | E10 | E13 | E16 | E20 | E25 |
|-------------|-------|-----|-----|------|------|
| 30 kHz | 1.5 W | 2 W | 4 W | 7 W | |
| 60 kHz | 3 W | 4 W | 6 W | 13 W | 25 W |
| 115/120 kHz | 5 W | 6 W | 8 W | 18 W | 32 W |

- Basic specification of transformer include
 - Size, isolation barrier, reflected voltage, peak (or saturation) current, frequency, input voltage range, output voltage and output current range
- Leakage inductance influence power loss, snubber and EMI
 - Typical leakage inductance is 1~3% of primary inductance depending on the transformer structure
 - $P_{Leakage} = \frac{1}{2} L_{Leakage} I_P^2 \times f_s$
- Reflected Voltage V_R is the voltage reflected from secondary output to the primary of transformer

Minimizing L_{leakage} by Interleaving

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- Leakage inductance can be reduced by splitting primary winding in 2 halves and sandwiching secondary winding in between



Reflected Voltage Selection

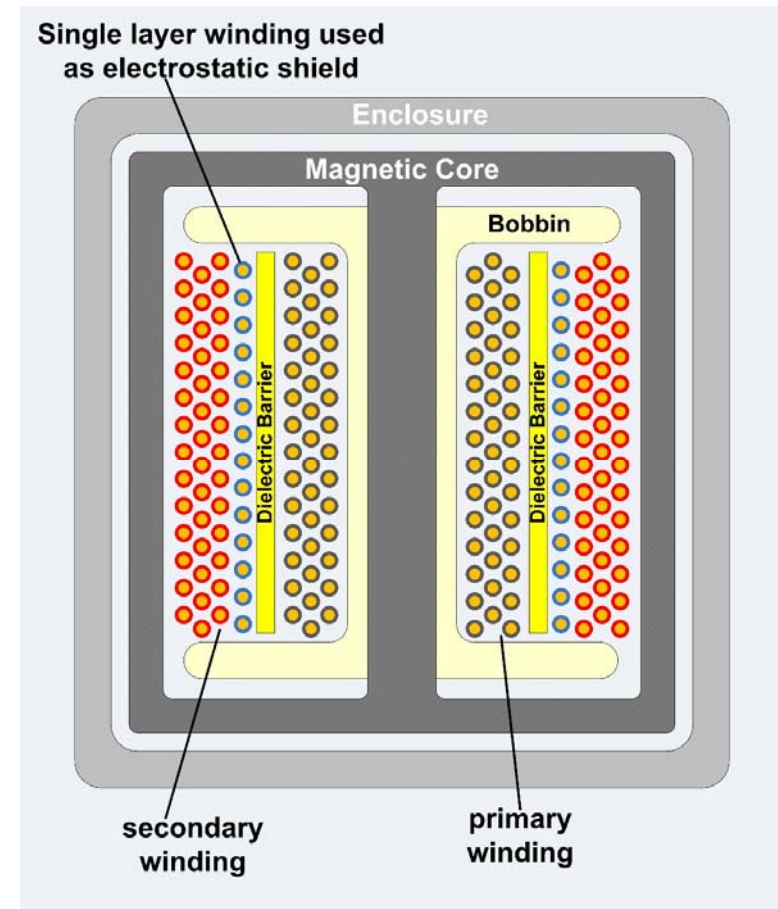
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- Optimize reflected voltage to set maximum duty cycle. As a rule of thumb, make it equal to minimum DC input voltage
- High reflected voltage means high V_{ds} stress and higher snubber losses
- Lower reflected voltage means higher off time, higher RMS losses and higher primary peak current
- A positive side effect of lower reflected voltage is that it leads to better magnetic coupling between windings, which, in turn, helps to reduce leakage inductance
- On the other hand, consider that a lower reflected voltage involves higher primary peak currents at heavy load

Shielded or Non-Shielded

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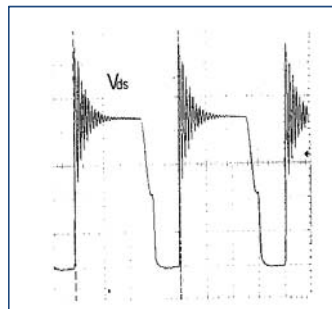
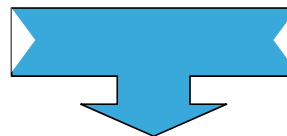
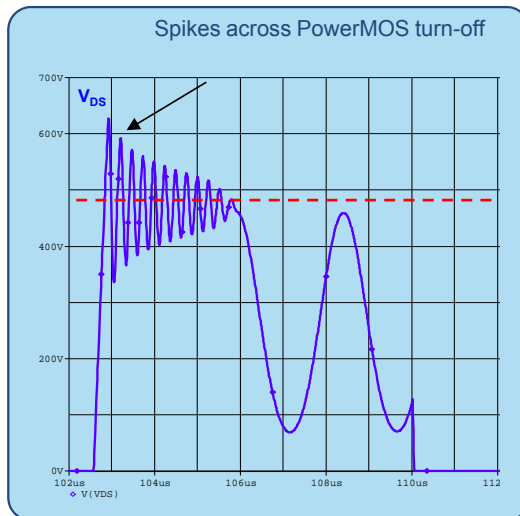
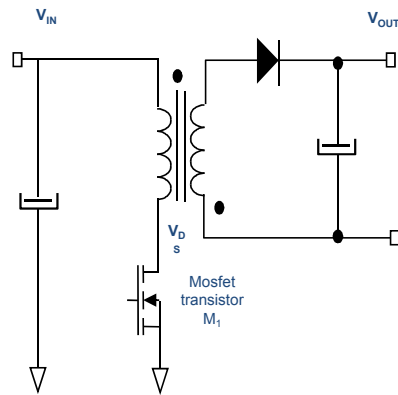
- Shielded transformer has better EMI but larger leakage inductance
- Non-shielded transformer has worse EMI but smaller leakage inductance



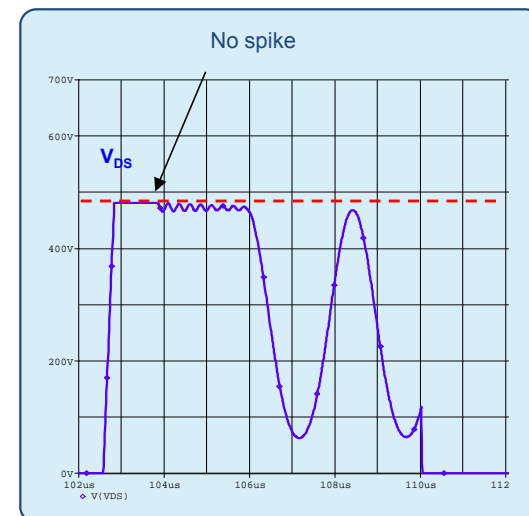
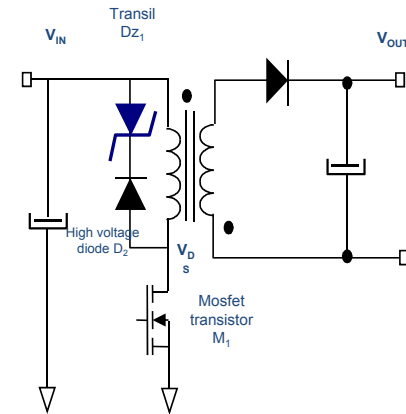
Clamp Circuit

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Without Clamp Circuit

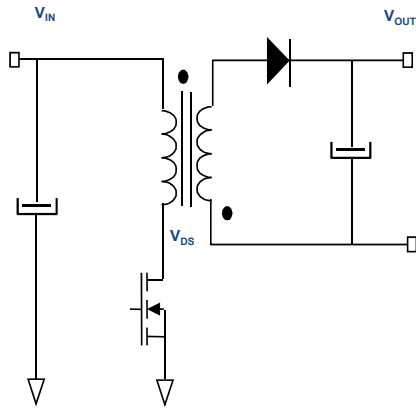


With Clamp Circuit

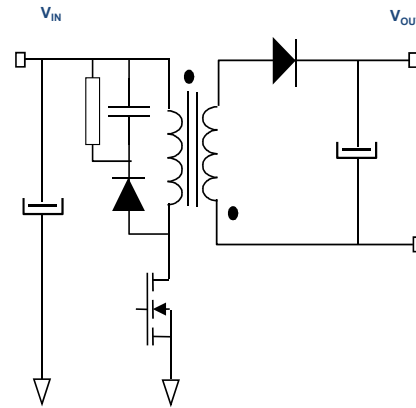


Clamp Implementations

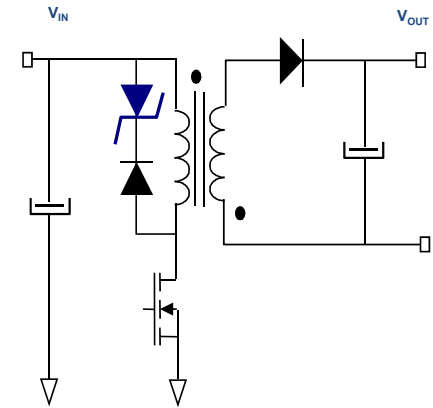
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- No protection
- Test to be performed to know max V_{DS}
- MOS / IGBT to be oversized in voltage (more expensive, efficiency drop)



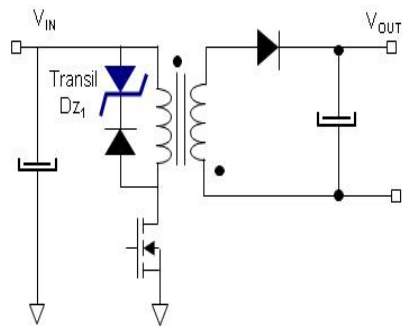
- RC to limit dV/dt , then to limit overvoltage
- Slope may vary depending on components
- Margin on V_{DS} is depending on components
- Test to be done for validation



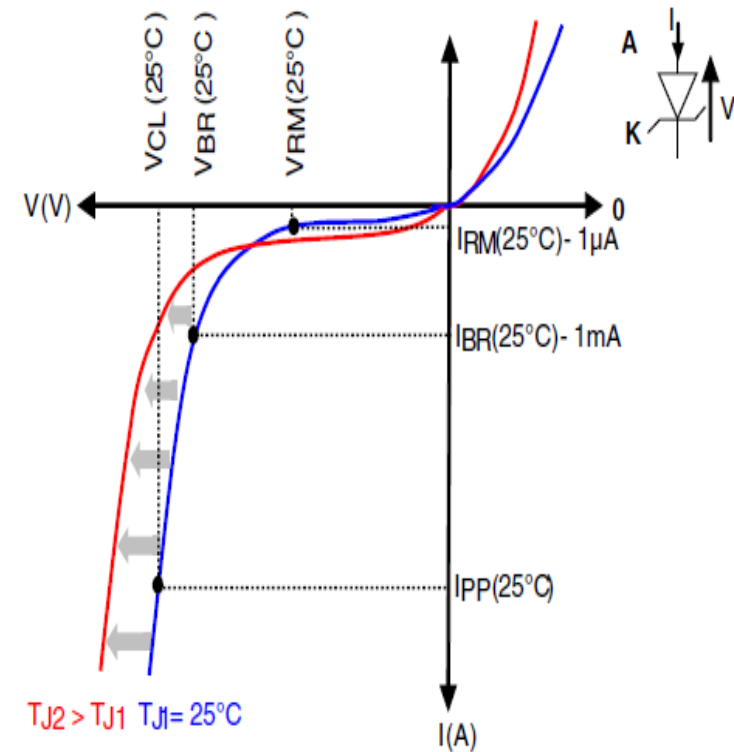
- Maximum clamping voltage only depends on STRVS
- Datasheet/product adapted to repetitive surges
- Margin on V_{DS} can be easily calculated
- Validate with minimal test

New Clamping Technology: STRVS

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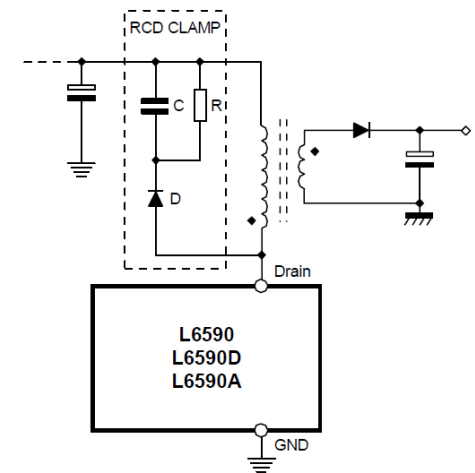
- VRM is stand-off voltage and must be selected to allow the FET to switch: $VRM > V_{IN} + VR$
- VCL is the clamping voltage and is critical to choose as close as possible to the application requirement
- Extensive data published on STRVS datasheet makes the selection for the right part easy and robust



RCD Snubber

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- RCD sizes and values need to be carefully selected. There is a tradeoff between RC values, power dissipation, EMI and clamping effect
- RCD clamp dissipates power even under no-load conditions: there is always the reflected voltage across the clamp resistor R



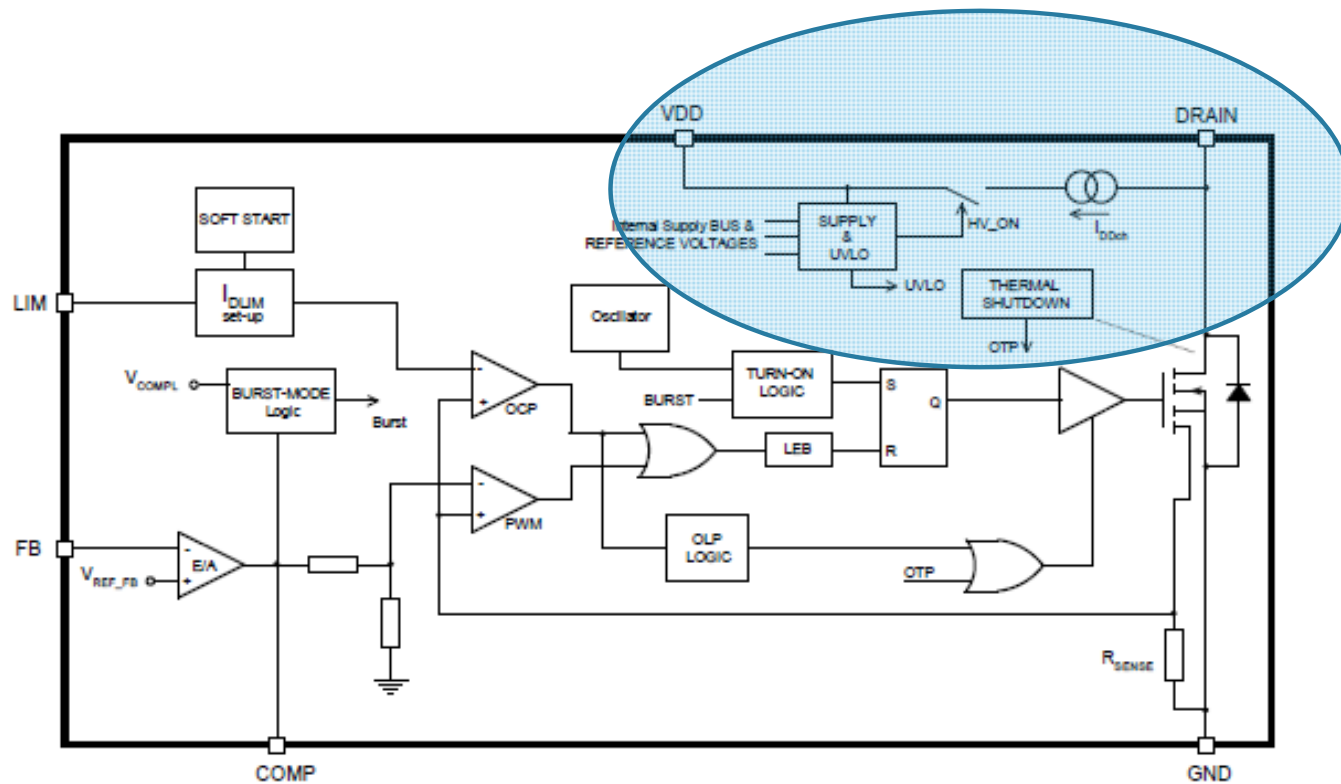
| R | C | V_{CL} | $V_{DS(PK)}$ | EMI | $P_{DISS(R)}$ | Cost |
|---|---|----------|--------------|-----|---------------|------|
| ↑ | ↑ | ↓ | ↓ | ↓ | ↑ | ↑ |
| ↓ | ↓ | ↑ | ↑ | ↑ | ↓ | ↓ |

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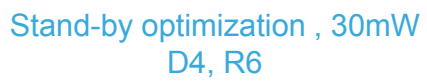


Stand-By Consumption: HV Start-Up

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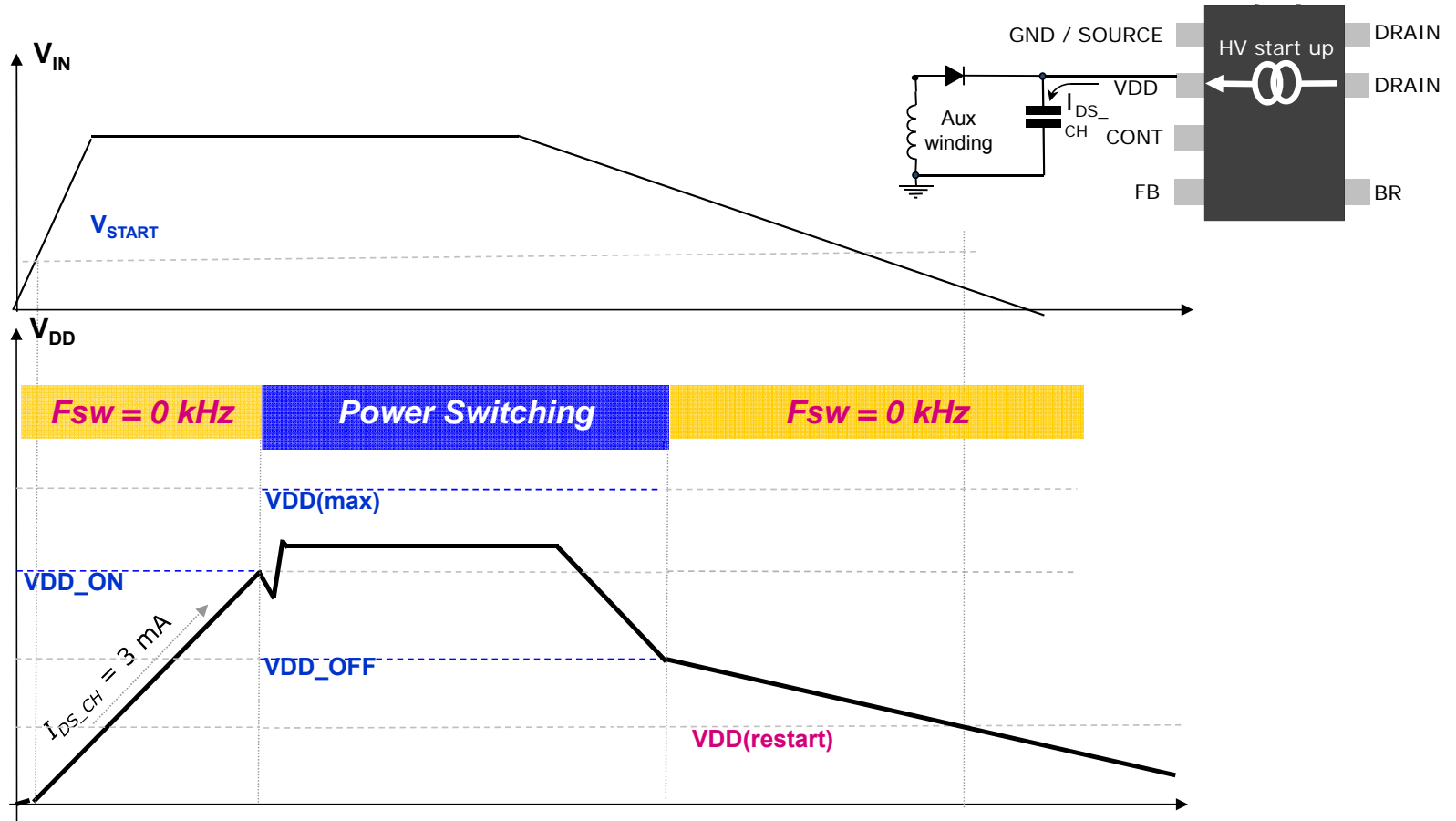


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Stand-By Consumption: HV Start-Up

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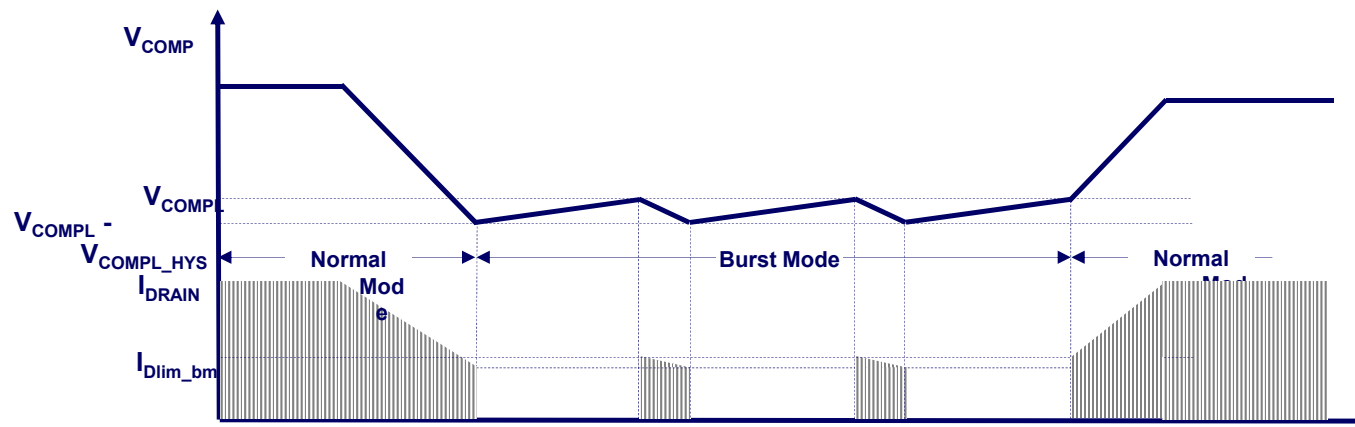


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Stand-By Consumption: Burst Mode

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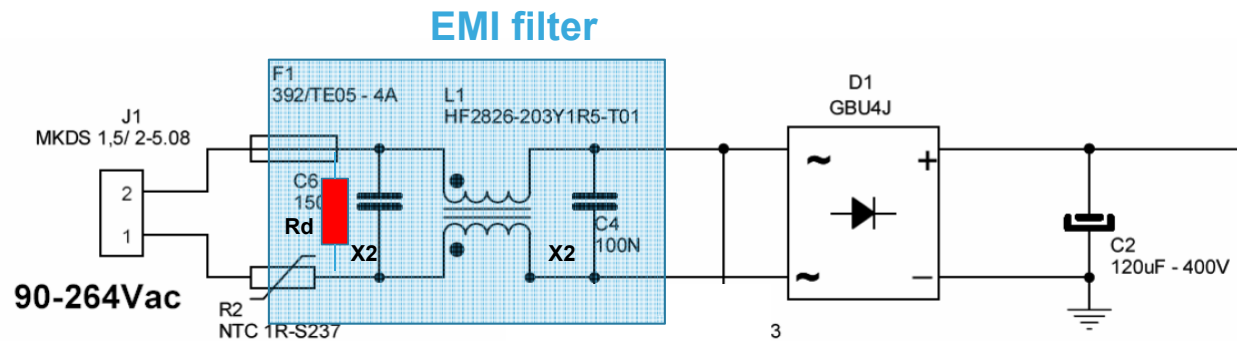


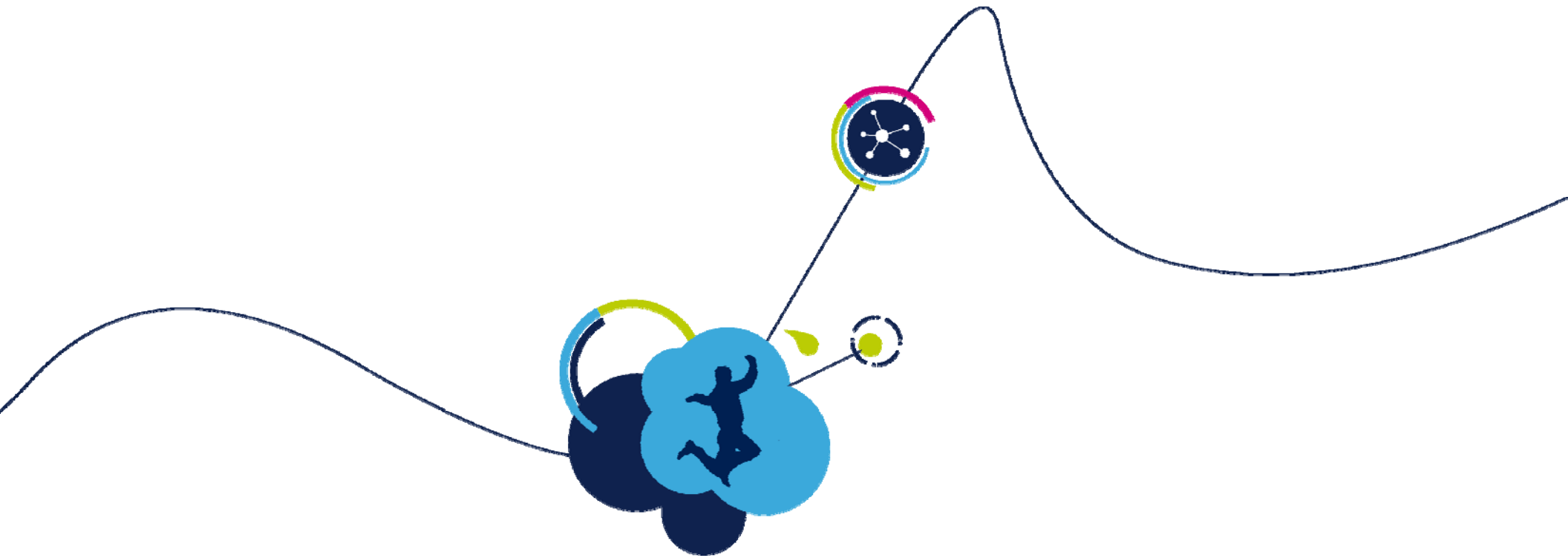
$V_{COMP} < V_{COMPL}$ starts burst mode

X-Cap Discharge

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- The EMI filter in the input of the power converter typically consists of capacitors across the AC mains and CM choke
- According to safety regulations, e.g. UL 1950 and IEC61010-1, capacitors on the mains must be discharged within a given time after the appliances is suddenly disconnected
- A discharge resistor is typically connected in parallel, resulting in additional power losses, as long as the appliance is plugged
- An new function has been recently introduced in order to actively discharge the X capacitor through the HV start-up circuit

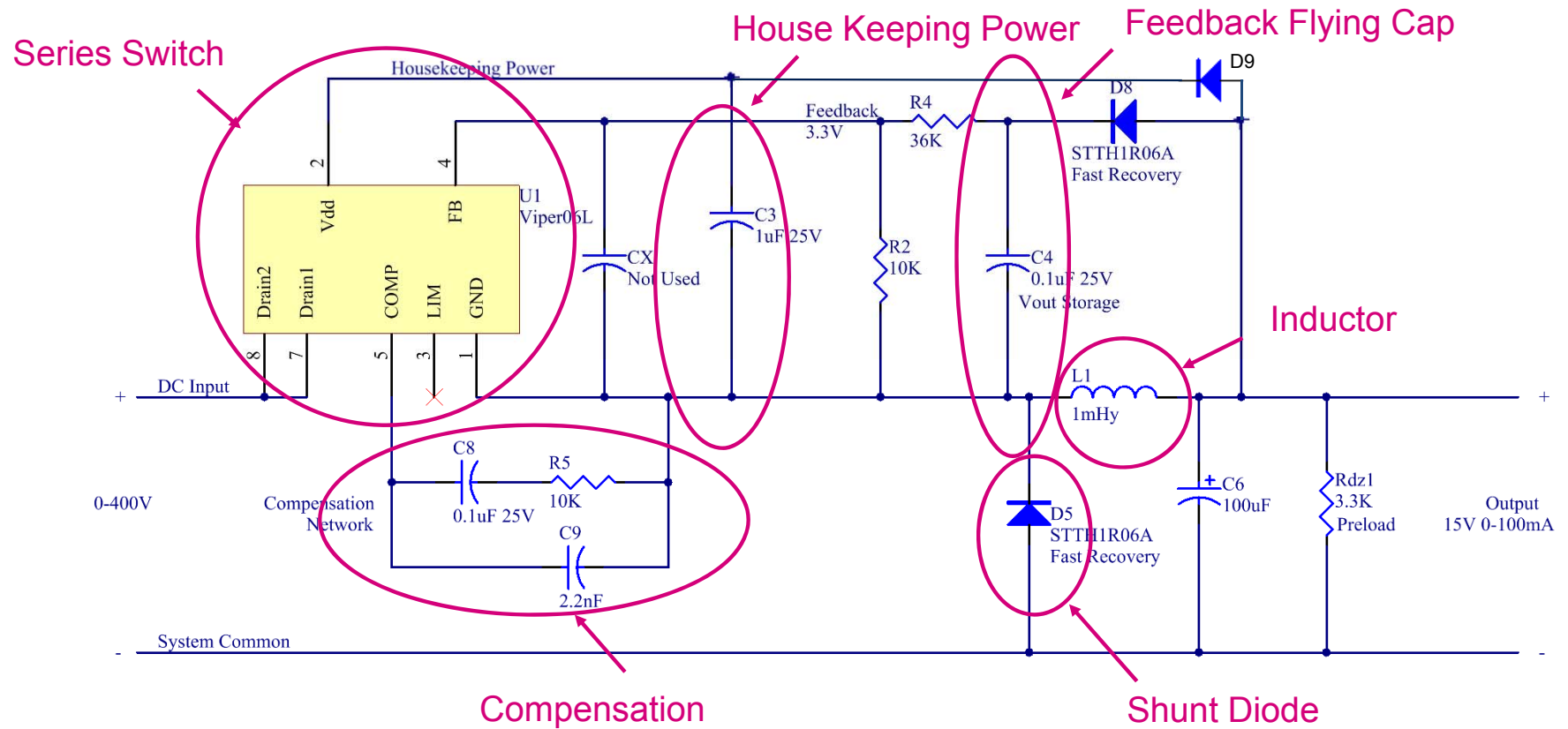




Buck Topology Optimization

Buck Schematic

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“Flying Capacitor” Feedback Scheme

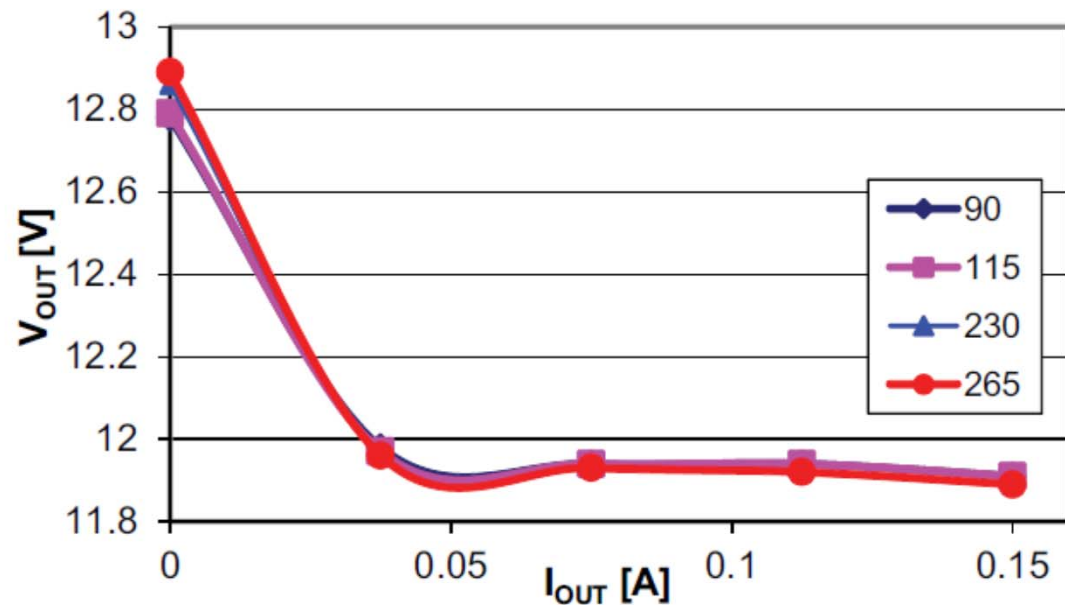
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- C4 stores output voltage, transfers level into Viper feedback loop
- R4 – R2 discharge C4 slowly
- Load current is required to turn on D5 and D8 to charge C4
- A light load MUST be present to insure diode turn-on
- C4 must hold output voltage information when Viper is in burst mode

“Flying Capacitor” Feedback Scheme (Cont.)

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- Low cost solution
- Minimum load required



Select Switching Frequency

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SELECT FREQUENCY FOR 5 V OUTPUT BUCK

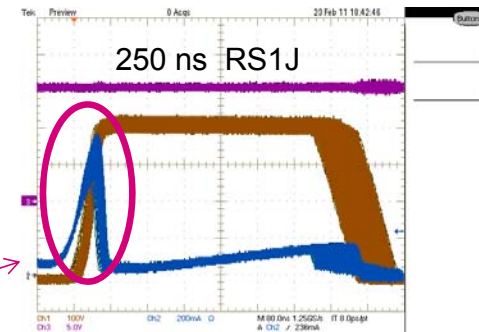
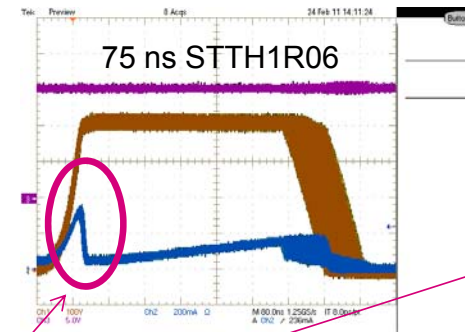
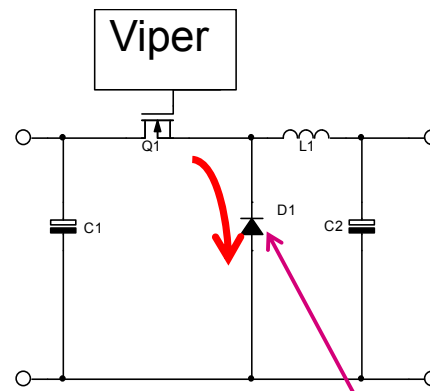
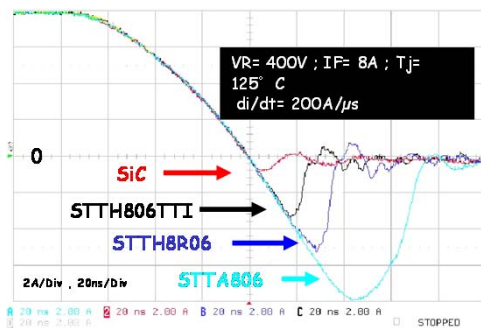
| Vin DC (V) | D (%) 5 V | t _{ON} (μs) for 60 kHz 5 V | t _{ON} (μs) for 30 kHz 5 V | VIPer01 Minimum ON time |
|----------------|-----------|--|--|-------------------------------|
| 100 (85 VAC) | 5.0 | 0.83 | 1.67 | 0.35 μs |
| 170V (120 VAC) | 2.9 | 0.49 | 0.97 | |
| 325V (230 VAC) | 1.5 | 0.26 | 0.50 | |
| 375V (265 VAC) | 1.3 | 0.22 | 0.33 | |
| 622V (440 VAC) | 0.8 | 0.13 | 0.26 | |

Lower frequency allows to handle the regulation even in the case of a very high ratio between input and output voltages

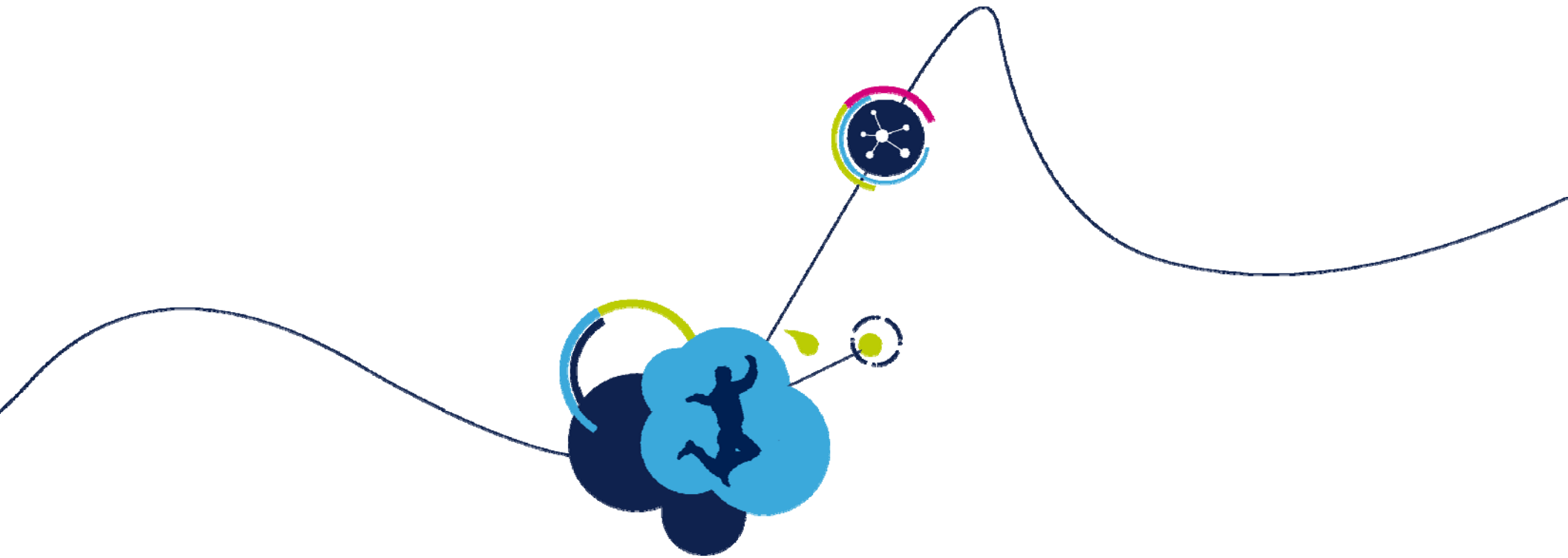
Minimum ON Time 31

- Duty cycle of Viper Buck converter is limited by minimum on time
 - Viper06 450 ns
 - Viper01 350 ns
- If the required ON time is shorter than minimum ON time, Buck still works, but there is small instability and the maximum deliverable output current is reduced.
- The 30kHz version is strictly recommended for 5V output

Diode Recovery Effect 32



Recovery effect causes short cross conduction ever turn ON. Effect is much critical in case CCM => **DCM is recommended**. The lost energy is higher at higher power operating frequency => **The 30kHz version is recommended.**



Layout and EMI Optimization

Layout Optimization

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- Minimize interconnection lengths of following components:
 - Input filter caps, input-side transformer (or inductor), power MOSFET, sensing resistors and active-clamp or snubber circuits
 - Output-side transformer (or inductor), rectifier diodes and output filter caps
- Keep power and signal circuitries separated and careful of connection between the signal and power grounds
- Assure component isolation and spacing by safety standards
- Prioritize ground over all routes
- Compromise copper areas between Thermal and EMI
- Add sufficient VIAs for better thermal performance
- Keep the feedback path as far as possible from power components and noise traces
- External compensation components should be close to IC
- Copper traces for power should be thick and short and sharp angles should be avoided

EMI Optimization

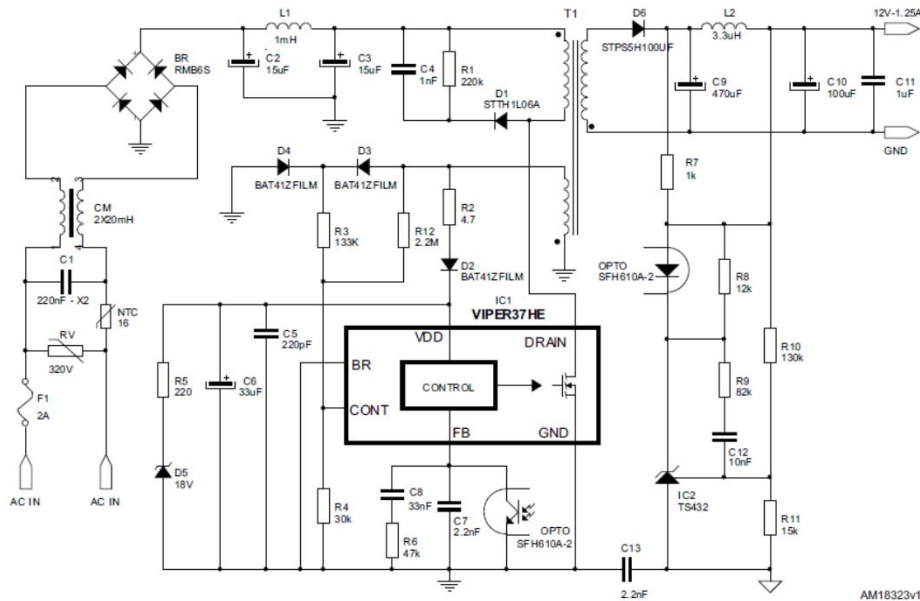
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- EN 55022 is an European EMC standard applicable to information technology equipment with a rated supply voltage not exceeding 600 V
- Properly size EMI filter: differential mode filter for power < 5 W; X-, Y-caps, and common mode choke for power > 15 W
- Designers often use snubbers and soft switching techniques to minimize the EMI
- Shielded transformer has better EMI but also has larger leakage inductance
- Connect heatsinks to ground
- Focus on coupling paths from EMI sources to EMI sensitive components
- Strategic orientation and placement of components can reduce EMI generation significantly
- Eliminate environmental interference on EMI test
- Use an accurate EMI analyzer to carry quasi-peak, and average measurement to meet standards
- ST offers PWM operation with frequency jittering for low EMI

Design Example

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Electrical Schematic



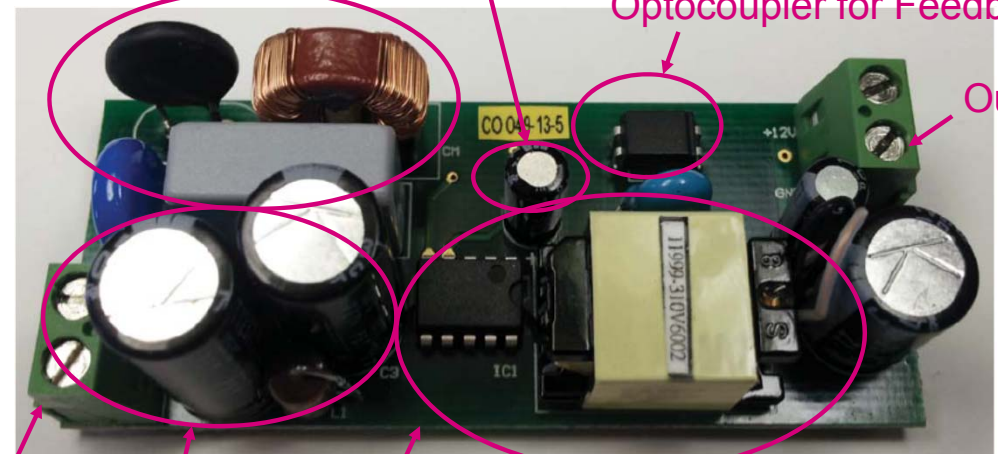
VIPER37HE 100~265 VAC IN, 12 VDC 15 W OUT

EMI Filter

Aux VDD for Viper

Optocoupler for Feedback

Output



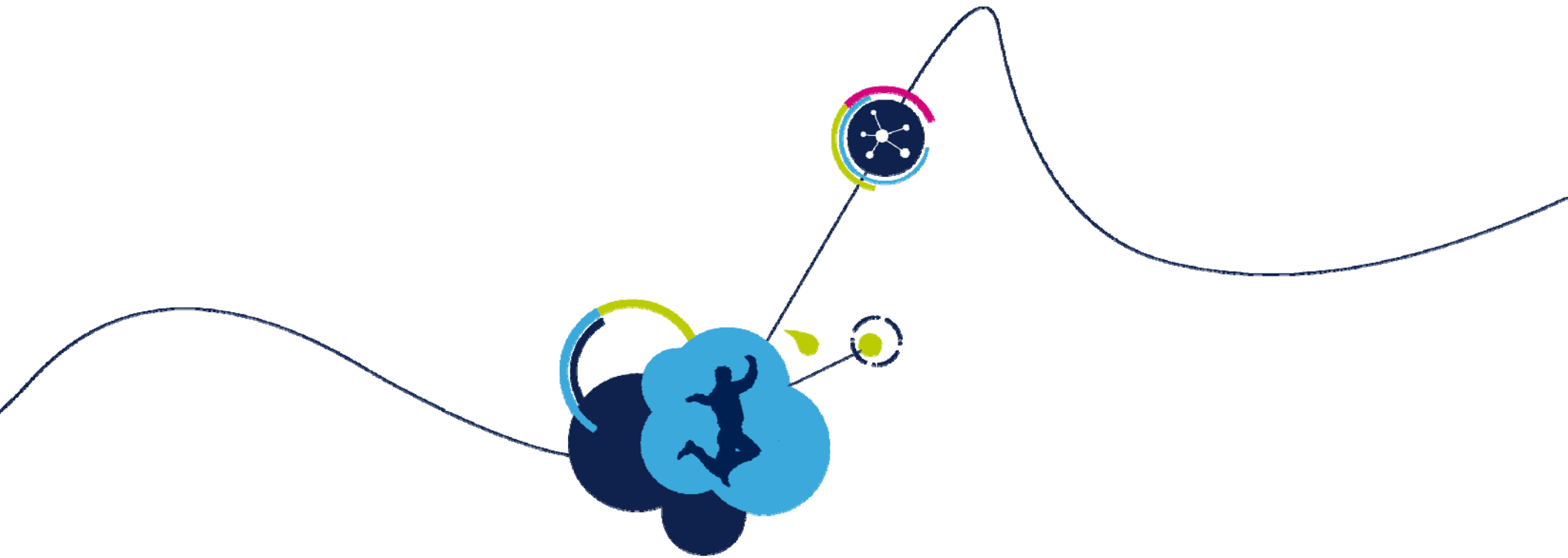
Input

Rectifier

Subber and Comp
(Bottom Layer)

Compact Power Loop

Evaluation Board (30 x 72 mm) Max



eDesignSuite Examples

eDesignSuite

The smart tool to design your application



Power Supply
DC/DC - AC/DC



LED Lighting
DC/DC - AC/DC



Photovoltaic
DC/DC



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AC/DC



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1

2

3

4

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The specifications view

The actuals view

A full set of analysis diagrams

A full set of commands

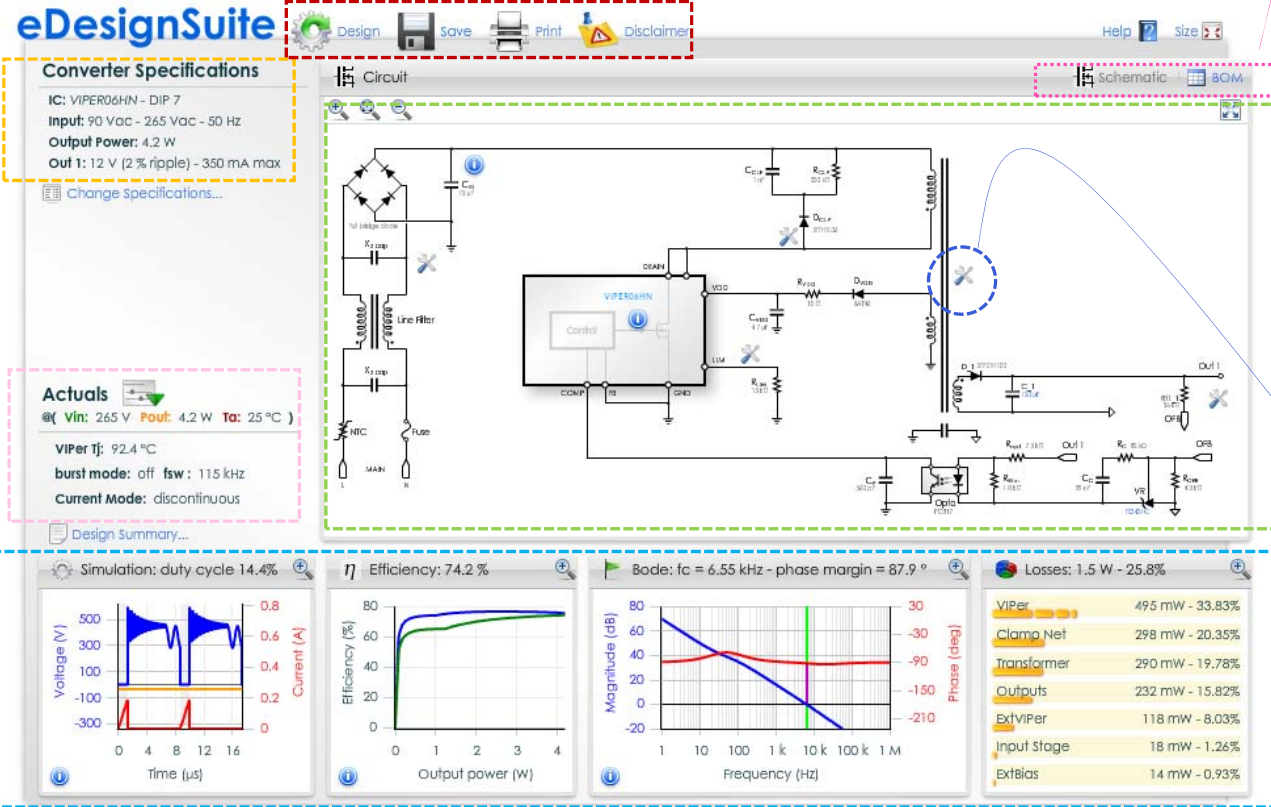
A fully and interactive BOM

A fully annotated and interactive schematic

The user can customize the Flyback transformer

The design view

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Thank you !