

Extremely accurate timekeeping over temperature using adaptive calibration

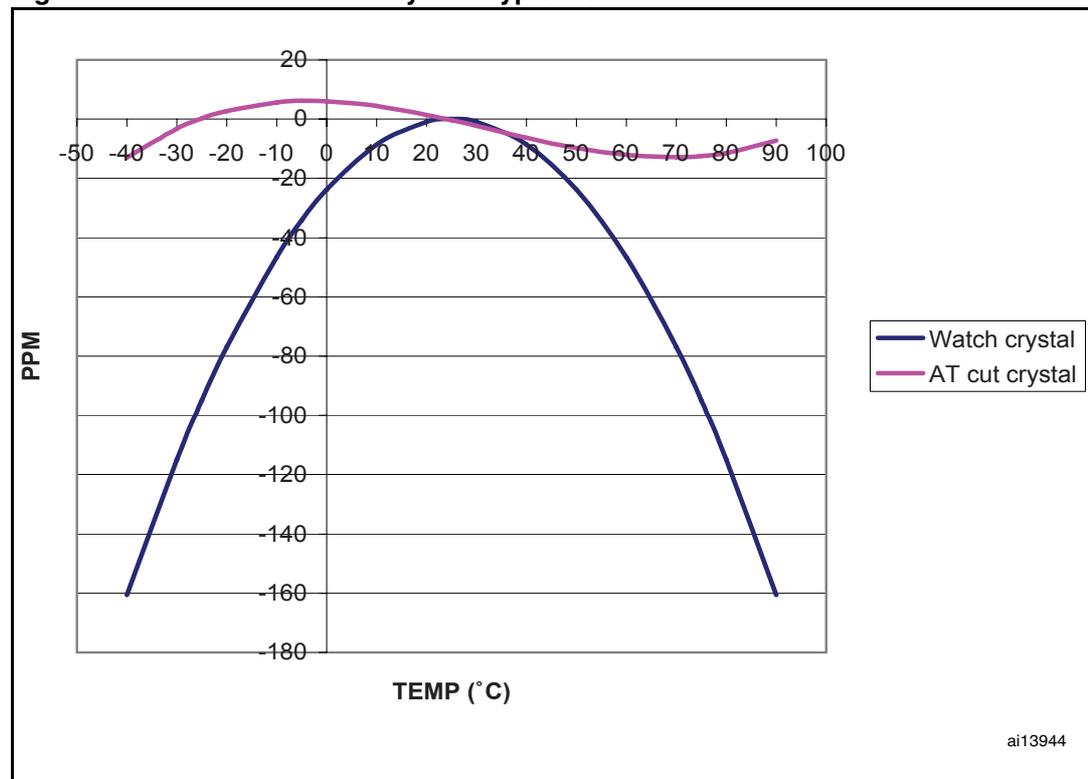
Introduction

Typical real-time clocks use common 32,768 Hz watch crystals. These are readily available and relatively inexpensive, but they suffer a loss of accuracy when operated over wide temperature ranges. However, the ultra-low power characteristics of 32 KHz oscillators make them ideal, and necessary, for battery backed applications.

Conversely, the higher speed, AT-cut crystals used with microprocessors have low drift over a wide temperature range, and can thus provide high accuracy, but their oscillators are not suitable for backup since they will draw much more current at the frequencies common with AT-cut crystals.

The purpose of this application note is to show how, using a combination of these crystal characteristics, users can get high accuracy over a wide temperature range using ST's M41T82-83-93 series of RTCs. This is accomplished by first measuring the frequency and then using both the analog and digital calibration features of these devices.

Figure 1. AT versus watch crystal - typical characteristics



1 M41T82-83-93 series RTCs

ST has long offered RTCs with digital calibration, and the new M41T82-83-93 series follows suit. In addition to digital calibration utilizing periodic counter correction, this new series features analog calibration wherein the oscillator frequency can be adjusted by adding or removing load capacitance via a programmable capacitance array. Analog calibration has the added benefit of instantaneous feedback for the user; adjustments to the oscillator speed are immediately visible in the 512 Hz test output signal built into the devices.

1.1 Oscillator temperature characteristics

As shown in [Figure 1](#), the frequency error of typical 32 KHz oscillators is around -25 parts per million (ppm) at both 0°C and 50°C . That is, at 25° above and below room temperature, the device exhibits a frequency deviation of -25 ppm, and it only gets worse as the temperature deviates farther from $\pm 25^{\circ}\text{C}$.

Conversely, for an AT cut crystal, as is commonly used with microprocessors, the frequency deviation is much less pronounced over a wide range of temperatures. The trade-off is that AT cut crystals usually operate at frequencies much, much higher than watch crystals and thus require much more power - too much for battery backup as is typically employed with real-time clocks (RTCs).

But it is possible to get the low power performance of watch crystals along with the wide temperature accuracy of AT cut crystals if the RTC can be periodically calibrated by the microprocessor, almost all of which nowadays include timers that can be employed to measure the frequency test (FT) pin of the RTC and correct any error in the timing utilizing the calibration features of the RTC.

The approach discussed herein utilizes both of the calibration circuits in ST's M41T82, M41T83 and M41T93 serial RTCs. This application note describes how to perform an initial calibration, using the analog circuit, followed by occasional calibration updates using the digital calibration circuit.

Initially, the analog calibration circuit is adjusted at room temperature, in a closed loop fashion wherein successively smaller and smaller adjustments are made until the error is minimized. After that, during normal operation, the microprocessor will periodically measure the error as before, then use a look-up table, and write adjustments to the digital calibration circuit.

1.2 Frequency test output

In the case of ST's M41T82, M41T83 and M41T93 serial RTCs, the frequency test signal is output on the $\overline{\text{IRQ}}/\text{FT}/\text{OUT}$ pin. It is enabled by setting the FT bit (bit 6, register 0x08) to 1 in the M41T82 and M41T83. (Refer to the datasheets for more information and for the M41T93 details.) The FT signal is measured by test equipment and/or the microprocessor. The calibration circuits are then adjusted accordingly.

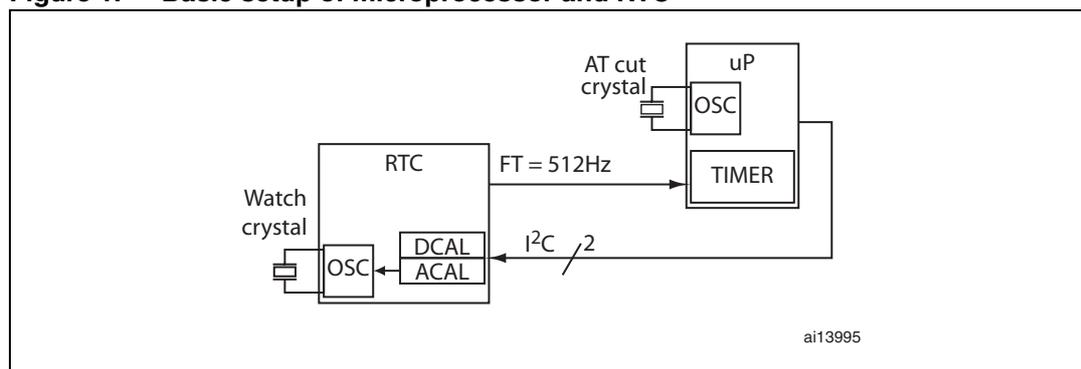
The frequency test signal is nominally 512 Hz and is derived from the 32,768 Hz oscillator. During the analog calibration sequence, changes in the oscillator will appear in real-time in the FT signal. Thus, analog calibration changes can be measured and errors can be minimized on-the-fly by the system microprocessor.

1.3 Measuring FT and the timing error

For the analog calibration, a frequency counter is recommended. This will provide the highest accuracy. The next consideration is using the microprocessor's timer. This can be used to adjust the analog calibration and will be used for the digital portion.

Microprocessor timers can come in a variety of configurations with many different speeds and input options, so this document can only address them in a general sense. [Figure 1](#) shows the basic setup between the RTC and the microprocessor. The processor's timer is used to measure the frequency of the RTC's frequency test signal (FT) and then adjust the RTC's calibration registers as necessary via the I²C bus.

Figure 1. Basic setup of microprocessor and RTC



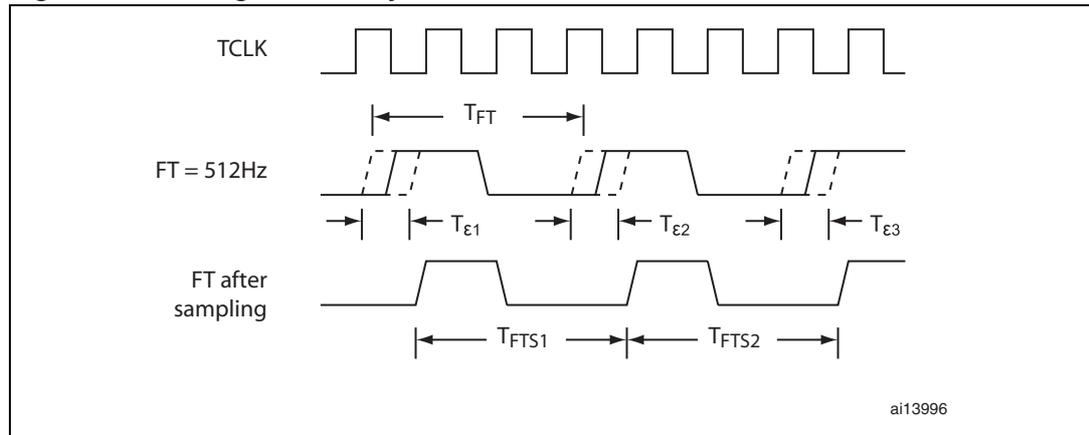
Fundamentally, the processor needs to measure the period of the timer and calculate the error or frequency deviation of the FT signal, but the measurement process is itself prone to error. However, it should be possible to minimize that error to an acceptable level.

The key concept is that the microprocessor's timer runs off a clock signal derived from the microprocessor's oscillator with AT cut crystal. Since this oscillator has low drift over temperature, the timer's clock signal will be low drift, too. Thus, using this timer, the RTC can be calibrated to approach the accuracy of this timing chain, thus reducing the timekeeping errors associated with watch crystals due to temperature drift.

In [Figure 2](#), the microprocessor's clock is called TCLK, and is used to sample the 512 Hz frequency test signal, FT. Each sample includes some uncertainty. But the uncertainty does not change as more samples are added. Thus, with many samples, the uncertainty will be very small in comparison to the measured period.

For example, in [Figure 2](#), the timer can detect that a transition occurred on the FT signal between two successive samples, but it cannot determine exactly where between those samples that it occurred. That uncertainty is labeled $T_{\epsilon 1}$, $T_{\epsilon 2}$ and $T_{\epsilon 3}$ in the figure.

Figure 2. Timing uncertainty



The first cycle of the sampled (bottom) waveform has the period

$$T_{FTS1} = T_{FT} + T_{\epsilon 2} - T_{\epsilon 1}$$

Similarly, the second cycle has the period

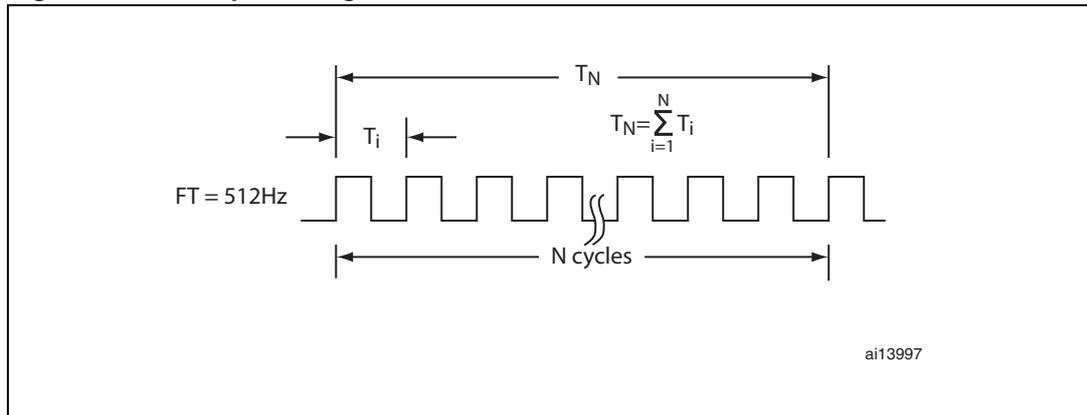
$$T_{FTS2} = T_{FT} + T_{\epsilon 3} - T_{\epsilon 2}$$

For both cycles together, the total period is

$$T_{FTS1} + T_{FTS2} = 2 \times T_{FT} + T_{\epsilon 2} - T_{\epsilon 1} + T_{\epsilon 3} - T_{\epsilon 2} = 2 \times T_{FT} - T_{\epsilon 1} + T_{\epsilon 3}$$

This shows that the uncertainty between all the samples (except the first and last) subtracts out of the total with the result that only the uncertainty of the first and last cycles remains. Thus, the net uncertainty will be small compared to the overall measured period, T_N , of multiple samples of the 512 Hz signal, as shown in [Figure 3](#). So, by measuring several consecutive samples of the 512 Hz signal, the uncertainty can be minimized to an acceptable level.

Figure 3. Example timing



1.4 Calculating the period

As shown in [Figure 3](#), the microprocessor will measure multiple cycles of the FT signal to get a total period, T_N. The calculated period of the 512 Hz is then

$$T_{512} = \frac{T_N}{N} = \frac{\sum_{i=1}^N T_i}{N}$$

If N is sufficiently large, the uncertainty error, T_{εN} – T_{ε1}, can be ignored.

The microprocessor's timer will measure the T_i, the period of each sample. Either software or some other timer function, such as a pulse accumulator, available on many microprocessor timers, will count the number of samples, N. Likewise T_N is the sum of the T_i, and can be accumulated in a timer function or in software. Once these are determined, software will then calculate T₅₁₂ by dividing T_N by N.

1.5 Determining the error

The error formula, in ppm, where f_m is the measured frequency, is below. When using a frequency counter, this can be used to determine the error.

$$\text{ppm} = \frac{f_m - 512}{512} \times 10^6$$

The formula below can be used to determine the error when using the microprocessor timer to determine the period, T_{512} , of the frequency test signal.

Equation 1

$$\text{ppm} = \frac{\frac{1}{512} - T_{512}}{T_{512}} \times 10^6$$

A negative ppm means the frequency is too low and the clock is slow. Conversely, a positive ppm means the clock is fast and thus needs to be slowed down.

2 Calibrating the M41T83 using analog calibration

The analog calibration procedure is performed only once, at room temperature (25°C). It begins with determining the frequency test signal's period, T_{512} . Then, the software adjusts the RTC oscillator via the analog calibration feature, and another measurement of T_{512} is made. This cycle is repeated until the error is minimized, that is, until the oscillator can be fine tuned no further. At that point, the RTC's accuracy will be approximately equal to the microprocessor's oscillator accuracy, which, depending on the quality of its crystal, may not vary more than ± 5 ppm over a wide temperature range.

2.1 Analog calibration circuit

The analog calibration circuit utilizes an array of load capacitors internal to the RTC as shown in the inset of [Figure 4](#).

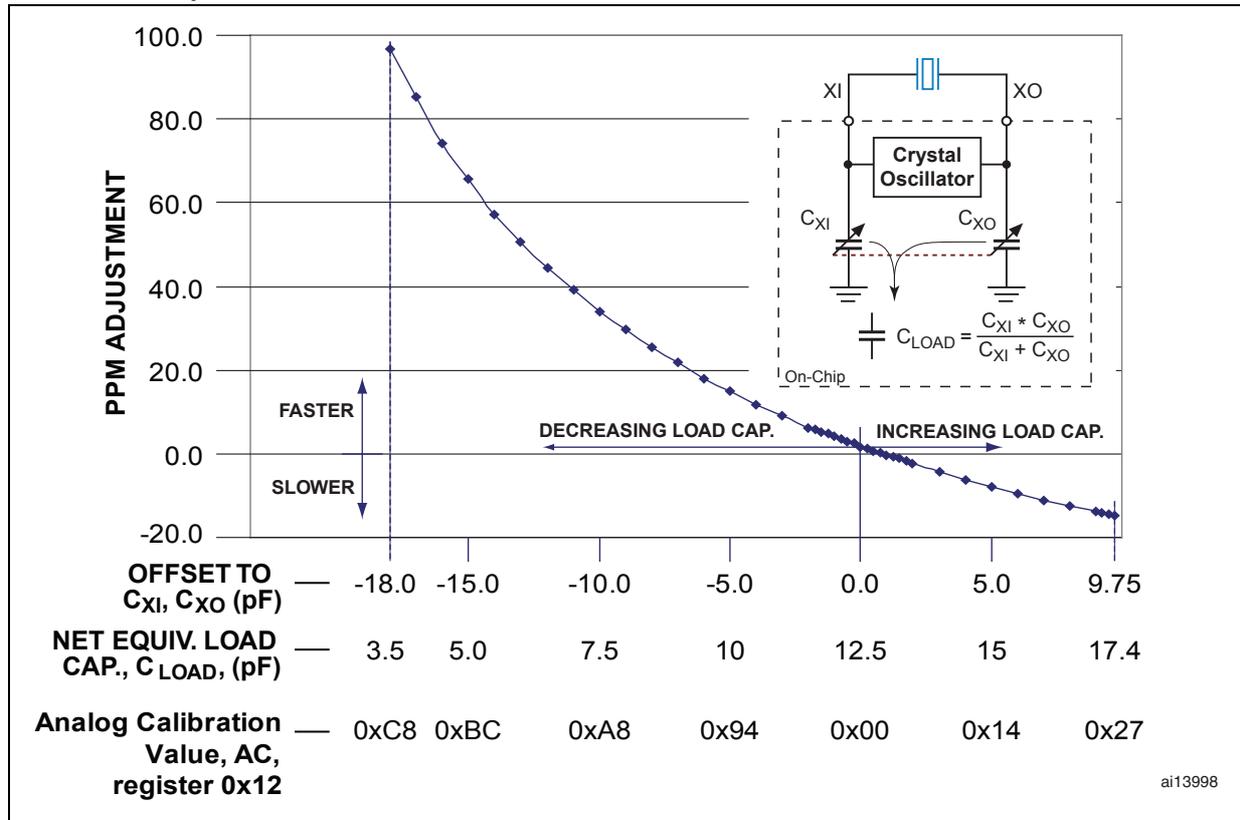
Values written to the analog calibration register add or remove load capacitance to slow down or speed up the oscillator, respectively. The 32 KHz crystals are designed to see a specific load capacitance. ST builds this into their real-time clocks; users do not need to add any external capacitance to the crystals. Values programmed into the analog calibration register adjust the amount of this built-in load capacitance seen by the crystal.

As shown in [Figure 4](#), two load capacitors are identified as C_{X1} and C_{X0} . Nominally, these are 25 pF each. The adjustment range of the RTC is such that up to 18 pF can be subtracted from each, or up to 9.75 pF can be added making the full range of each load capacitor 7 to 34.75 pF.

The equivalent load capacitance is the series combination of the two, and is hence nominally 12.5 pF with a range of 3.5 pF to 17.4 pF. (In other words, for identical capacitors, the series equivalent value is $\frac{1}{2}$ the individual values.)

The asymmetry in the adjustment range is due to the fact that the crystals tend to need speeding up much more often than they need slowing down. This is evident upon examining the watch crystal curve in [Figure 1](#). Thus, much more capacitance can be subtracted from nominal than can be added.

Figure 4. Typical analog calibration characteristics - oscillator frequency versus load capacitance



Associated with this range of capacitance values, the range of frequency shift of the oscillator is approximately -14.8 ppm up to +96.7 ppm. Several examples are shown in Table 1. This shift range corresponds to an approximate frequency range of 32767.514 Hz to 32771.168 Hz.

Table 1. Analog calibration examples

Analog calibration value	Hex	00	0C	14	27	9C	C8
	Bin	0000000 0	0000110 0	0001010 0	0010011 1	1001110 0	1100100 0
Additional load capacitance		0	+3 pF	+5 pF	+9.75 pF	-7 pF	-18 pF
Total load capacitance C _{XI} , C _{XO}		25 pF	28 pF	30 pF	34.75 pF	18 pF	7 pF
Total equivalent load capacitance C _{XI} in series with C _{XO}		12.5	14 pF	15 pF	17.4 pF	9 pF	3.5 pF
Approximate frequency shift		0 ppm	-4.3 ppm	-7.8 ppm	-14.8 ppm	+21.9 ppm	+96.7 ppm
	Nominal		←—Slowing down—→			←—Speeding up—→	

Thus, in summary, the nominal equivalent load capacitance is 12.5 pF, and can be adjusted up to 17.4 pF or down to 3.5 pF. This corresponds to slowing the oscillator by approximately -14.8 ppm or speeding it up by +96.7 ppm, respectively.

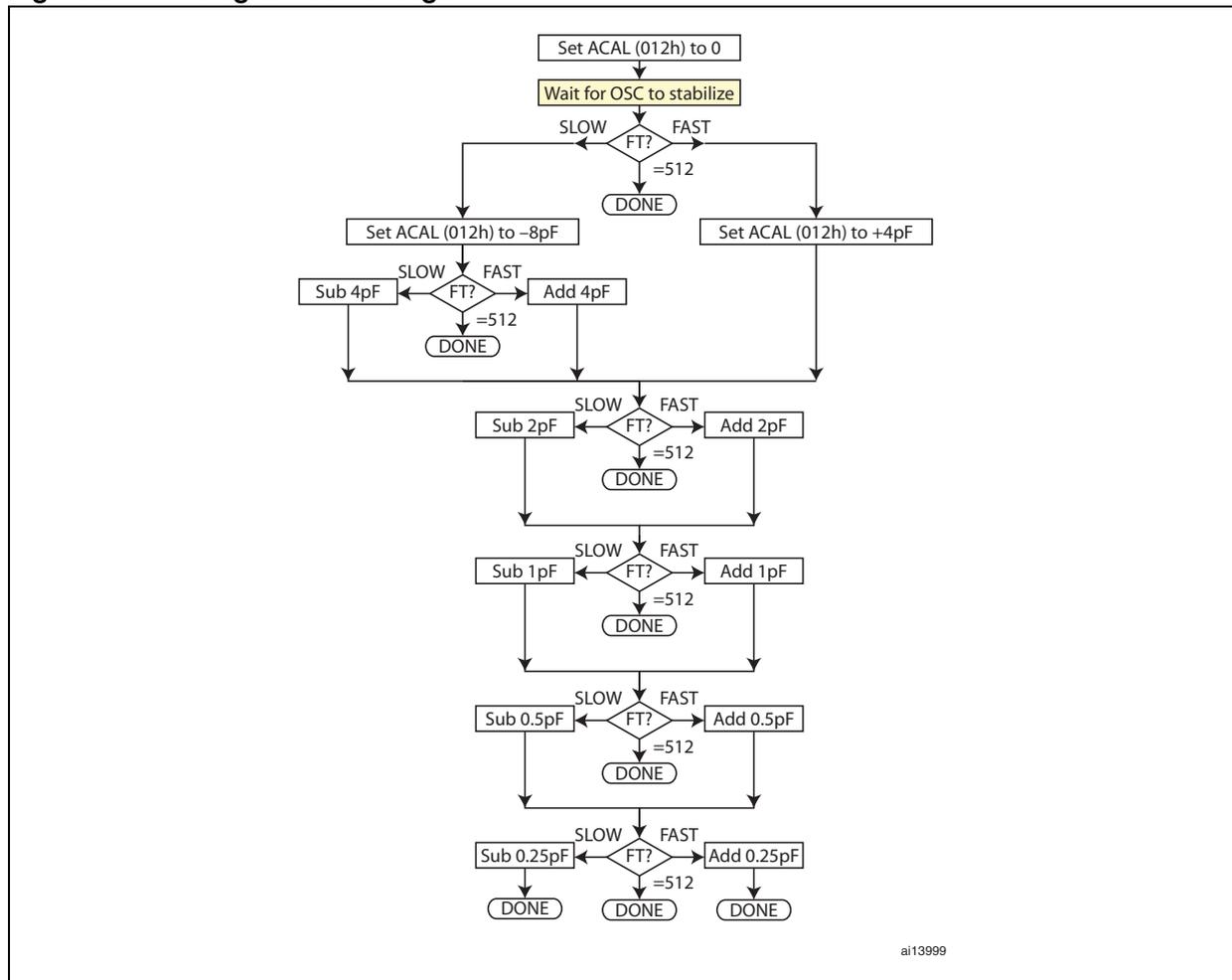
These are typical values. The curve in [Figure 4](#) may be shifted up or down, left or right for a given crystal. Because the curve is non-linear, an increment of capacitance at one operating point will not have the same effect as an equal increment at another operating point. Thus, table-lookup methods cannot be used with analog calibration. Instead, an iterative procedure is required to ensure accuracy.

2.2 Analog calibration algorithm

The analog calibration algorithm described herein uses a binary tree approach for adjustment. It utilizes repeated measurements as described in the scheme above. With each adjustment /measurement sequence, the RTC's oscillator is fine tuned with progressively smaller changes of the internal load capacitance array via the analog calibration register.

As shown in [Figure 5](#), the procedure starts with zeroing out the analog calibration register, then waiting a few milliseconds for the oscillator to stabilize. Next, the frequency measurement is made of the FT signal. If it is faster than 512 Hz, load capacitance is added to the RTC's oscillator. If it is slower than 512 Hz, capacitance is removed. And if the FT signal is exactly 512 Hz, no further adjustment is required.

Figure 5. Analog calibration algorithm



ai13999

As the watch crystal curve of [Figure 1](#) predicts, the RTC oscillator will tend to be slow more often than fast, so the adjustment range of the part is asymmetric; there is more range for increasing the RTC oscillator speed than for slowing it down.

For the M41T82, M41T83 and M41T93 RTCs, the smallest incremental adjustments are step sizes of approximately 0.25 pF. One step of 0.25 pF is roughly 0.5 ppm.

Since this algorithm uses a binary tree approach, each increment of capacitance must be a power of 2 times 0.25 pF. That is, capacitance will be added and/or subtracted in increments of 8 pF, 4 pF, 2 pF, 1 pF, 0.5 pF or 0.25 pF.

Thus, although up to 18.0 pF can be subtracted or up to 9.75 pF can be added, the power of 2 restriction constrains these limits to -16 pF and +8 pF, respectively. As a result, this algorithm does not use the total available adjustment range, but that will not be a problem in most applications.

For example, with this approach, when capacitance is to be added, instead of starting at half the maximum available, $\frac{1}{2} \times 9.75 \text{ pF}$ (= 4.875 pF), the power of 2 nearest that is used, which is 4 pF. Similarly, for removing capacitance, the most that can be subtracted is 18 pF, so the algorithm starts at the power of 2 nearest $\frac{1}{2} \times 18$, or 8 pF.

Returning to [Figure 5](#), after making the first measurement of FT, if capacitance is added, as shown on the right, the ACAL value is adjusted to 4 pF. Then, progressively smaller increments of capacitance are added or removed, until the frequency error measured on the FT pin is minimized.

If, in [Figure 5](#), the first test of the FT signal indicates that capacitance must be removed (that the RTC is slow), the analog calibration register is set to -8 pF and then progressively smaller increments of capacitance are added or removed.

Each time the analog calibration register is adjusted, the oscillator must be allowed time to settle before taking another measurement. This is shown at the top of [Figure 5](#), but not shown in successive steps for the sake of brevity. However, it is still required each time the register is written.

Using this binary approach, each of the 25 pF capacitors can be increased by up to 7.75 pF or decreased by up to 15.75 pF. While these adjustment limits are slightly less than the absolute limits available - up to a 9.75 pF increase or 18 pF decrease - they should cover all except the most extreme cases of RTC oscillator error.

It may be possible to use the wider, available adjustment limits in an adaptive calibration scheme like this one, but when increments other than powers of 2 are used, the algorithm becomes much, much more complex and thus may not be as easy for users to implement.

Once the final calibration bit has been determined, the user should record the value in non-volatile memory so that it can be retrieved by the microprocessor when necessary.

If a frequency counter was used to perform the measurements during the analog calibration procedure, the user should immediately follow that with the additional step of using the microprocessor and its timer to measure the period of the FT signal out of the real-time clock as described in [Section 1.3](#) and [1.4](#). This is done to establish the initial error, if any, in the microprocessor's timing chain at room temperature. This value should also be stored in non-volatile memory.

3 Digital calibration

The digital calibration feature of the M41T82, M41T83 and M41T93 uses periodic counter correction. The clock counters are adjusted by adding or subtracting pulses at the 512 Hz divider stage. This approach provides compensation over an approximate range of –63 ppm to +126 ppm.

This method employs the use of periodic counter correction by adjusting the ratio of the 100 Hz divider stage to the 512 Hz divider stage. Under normal operation, the 100 Hz divider stage outputs precisely 100 pulses for every 512 pulses of the 512 Hz stage. This 100 Hz signal is the input to the counter for the 10ths/100ths of seconds register in the RTC. By adjusting the number of 512 Hz input pulses used to generate 100 output pulses, the clock can be sped up or slowed down. To provide digital correction, the device will, depending on the digital calibration value, periodically produce one or more long or short seconds.

When a non-zero value is loaded into the five Calibration Bits (DC4 - DC0) of the Digital Calibration Register (0x08) and the sign bit is 1, (indicating positive calibration), the 100 Hz stage will output 100 pulses for every 511 input pulses instead of the normal 512. Since the 100 pulses are now being output in a shorter window, this has the effect of speeding up the clock by 1/512 seconds for each second the circuit is active.

Table 2. Digital calibration values

Calibration value, DC4-DC0		Calibration effect, in ppm, rounded to the nearest integer	
Decimal	Binary	Slowing Sign DCS = 0 negative calibration	Speeding Sign DCS = 1 positive calibration
0	00000	– 0 ppm	+ 0 ppm
1	00001	– 2 ppm	+ 4 ppm
2	00010	– 4 ppm	+ 8 ppm
3	00011	– 6 ppm	+ 12 ppm
4	00100	– 8 ppm	+ 16 ppm
5	00101	– 10 ppm	+ 20 ppm
6	00110	– 12 ppm	+ 24 ppm
7	00111	– 14 ppm	+ 28 ppm
8	01000	– 16 ppm	+ 33 ppm
9	01001	– 18 ppm	+ 37 ppm
10	01010	– 20 ppm	+ 41 ppm
11	01011	– 22 ppm	+ 45 ppm
12	01100	– 24 ppm	+ 49 ppm
13	01101	– 26 ppm	+ 53 ppm
14	01110	– 28 ppm	+ 57 ppm
15	01111	– 31 ppm	+ 61 ppm

Table 2. Digital calibration values (continued)

Calibration value, DC4-DC0		Calibration effect, in ppm, rounded to the nearest integer	
Decimal	Binary	Slowing Sign DCS = 0 negative calibration	Speeding Sign DCS = 1 positive calibration
16	10000	- 33 ppm	+ 65 ppm
17	10001	- 35 ppm	+ 69 ppm
18	10010	- 37 ppm	+ 73 ppm
19	10011	- 39 ppm	+ 77 ppm
20	10100	- 41 ppm	+ 81 ppm
21	10101	- 43 ppm	+ 85 ppm
22	10110	- 45 ppm	+ 90 ppm
23	10111	- 47 ppm	+ 94 ppm
24	11000	- 49 ppm	+ 98 ppm
25	11001	- 51 ppm	+ 102 ppm
26	11010	- 53 ppm	+ 106 ppm
27	11011	- 55 ppm	+ 110 ppm
28	11100	- 57 ppm	+ 114 ppm
29	11101	- 59 ppm	+ 118 ppm
30	11110	- 61 ppm	+ 122 ppm
31	11111	- 63 ppm	+ 126 ppm
N		-N/491520 (per minute)	+N/245760 (per minute)

Similarly, when the sign bit is 0, indicating negative calibration, the block will output 100 pulses for every 513 input pulses. Since the 100 pulses are then being output in a longer window, this has the effect of slowing down the clock by 1/512 seconds for each second the circuit is active.

The overall amount of calibration is controlled using the value (N) in the digital calibration register to generate the adjustments in one second increments. N is the number of affected seconds in the correction period. For positive calibration (speeding up), corrections are made to each of the first N seconds of every eight minute interval. For negative calibration (slowing down), corrections are made to each of the first N seconds of every 16-minute interval.

Thus, when speeding up, the first N seconds of every 480 second span (ie, every 8-minute span) are each slightly shorter. And when slowing down, the first N seconds of each 960 second span (ie, 16 minutes) are slightly longer.

To use the digital calibration feature, the measurement technique described in [Section 1](#) is used - the 512 Hz frequency test signal is measured by the microprocessor's timer.

Depending on whether this timer was also used to perform the initial analog calibration, an adjustment may need to be made to this number. Once the adjusted number is determined, the error in ppm is calculated and the appropriate offset from [Table 2](#) is selected and programmed into the digital calibration register.

Example 1: A frequency counter was used during analog calibration, and the subsequent period measured and calculated using the microprocessor's timer was 0.0019531441 seconds. Ideally, this number would be 0.0019531250 (= 1/512). Thus, the microprocessor's timer is about 10 ppm fast, and the earlier number, 0.0019531441, will be used in place of 1/512 in [Equation 1](#). Given a current calculated period of 0.0019531536, this is inserted into [Equation 1](#) for T_{512} , and the resultant error is -4.88 ppm. So the RTC should be adjusted by the opposite amount. In [Table 2](#), the positive value nearest this is +4 ppm, so the digital calibration register would get DCS = 1 and DC4:DC0 = 00001.

Example 2: The microprocessor's timer was used during analog calibration. As in example 1, let the calculated period be 0.0019531536 seconds. Inserting this into [Equation 1](#) (and retaining the 1/512), we get -14.65 ppm. The nearest opposite value is +16 ppm. For this, DCS = 1 and DC4:DC0 = 00100.

With digital calibration, the adjustments are made open-loop. In the case of the analog calibration adjustments, the frequency shift of the oscillator can be seen in the 512 Hz test signal, but with the digital calibration, the effects are spread out over time and are not immediately observable upon making changes. Furthermore, with digital calibration, no iteration is required. Once the frequency error is known, an appropriate value is programmed into the part and no further adjustments are made for while. The key idea is that adjusting the digital calibration requires one measurement followed by one adjustment; no looping is required.

This digital calibration procedure is repeated often enough to prevent the RTC from drifting too far, but no more often than every 16 minutes, the interval at which the RTC digital calibration algorithm updates. This can be reduced to 8 minutes when positive calibration values are being used. As the ambient temperature changes, the oscillator will drift, and the RTC oscillator will need adjustment. This can be done periodically by scheduling calibrations, or, if a temperature sensor is available to the microprocessor, by monitoring for changes in the temperature and adjusting the RTC when they occur. Or, a combination of both might be utilized. For example, scheduled RTC calibrations might occur every hour, and unscheduled ones might be run whenever a 2 degree temperature shift is detected.

As long as the microprocessor periodically adjusts the RTC, its timekeeping accuracy will be optimized, and timekeeping errors minimized.

4 Conclusion

By taking advantage of the analog calibration feature built into the new M41T82/83/93 family of serial RTCs, a low cost clock with high accuracy across temperature can be achieved. This approach requires only the use of the microprocessor timer to periodically measure the RTC's true frequency. Initially, the analog calibration is adjusted at room temperature. Then, periodic updates to the digital calibration register are made to compensate for any RTC oscillator drift due to temperature changes which may occur. During the analog calibration, a simple binary decision tree is employed which allows the user to fine tune the clock's oscillator and zero out any frequency shift. Subsequent digital calibration adjustments use a look-up-table.

Using this combination of analog and digital calibration enables the user to have a simple periodic update scheme which requires low overhead while providing accurate timekeeping and minimal cost.

5 Revision history

Table 3. Document revision history

Date	Revision	Changes
20-Dec-2007	1	Initial release.
26-Nov-2008	2	Updated <i>Figure 1</i> .

Please Read Carefully:

Information in this document is provided solely in connection with ST products. STMicroelectronics NV and its subsidiaries ("ST") reserve the right to make changes, corrections, modifications or improvements, to this document, and the products and services described herein at any time, without notice.

All ST products are sold pursuant to ST's terms and conditions of sale.

Purchasers are solely responsible for the choice, selection and use of the ST products and services described herein, and ST assumes no liability whatsoever relating to the choice, selection or use of the ST products and services described herein.

No license, express or implied, by estoppel or otherwise, to any intellectual property rights is granted under this document. If any part of this document refers to any third party products or services it shall not be deemed a license grant by ST for the use of such third party products or services, or any intellectual property contained therein or considered as a warranty covering the use in any manner whatsoever of such third party products or services or any intellectual property contained therein.

UNLESS OTHERWISE SET FORTH IN ST'S TERMS AND CONDITIONS OF SALE ST DISCLAIMS ANY EXPRESS OR IMPLIED WARRANTY WITH RESPECT TO THE USE AND/OR SALE OF ST PRODUCTS INCLUDING WITHOUT LIMITATION IMPLIED WARRANTIES OF MERCHANTABILITY, FITNESS FOR A PARTICULAR PURPOSE (AND THEIR EQUIVALENTS UNDER THE LAWS OF ANY JURISDICTION), OR INFRINGEMENT OF ANY PATENT, COPYRIGHT OR OTHER INTELLECTUAL PROPERTY RIGHT.

UNLESS EXPRESSLY APPROVED IN WRITING BY AN AUTHORIZED ST REPRESENTATIVE, ST PRODUCTS ARE NOT RECOMMENDED, AUTHORIZED OR WARRANTED FOR USE IN MILITARY, AIR CRAFT, SPACE, LIFE SAVING, OR LIFE SUSTAINING APPLICATIONS, NOR IN PRODUCTS OR SYSTEMS WHERE FAILURE OR MALFUNCTION MAY RESULT IN PERSONAL INJURY, DEATH, OR SEVERE PROPERTY OR ENVIRONMENTAL DAMAGE. ST PRODUCTS WHICH ARE NOT SPECIFIED AS "AUTOMOTIVE GRADE" MAY ONLY BE USED IN AUTOMOTIVE APPLICATIONS AT USER'S OWN RISK.

Resale of ST products with provisions different from the statements and/or technical features set forth in this document shall immediately void any warranty granted by ST for the ST product or service described herein and shall not create or extend in any manner whatsoever, any liability of ST.

ST and the ST logo are trademarks or registered trademarks of ST in various countries.

Information in this document supersedes and replaces all information previously supplied.

The ST logo is a registered trademark of STMicroelectronics. All other names are the property of their respective owners.

© 2008 STMicroelectronics - All rights reserved

STMicroelectronics group of companies

Australia - Belgium - Brazil - Canada - China - Czech Republic - Finland - France - Germany - Hong Kong - India - Israel - Italy - Japan - Malaysia - Malta - Morocco - Singapore - Spain - Sweden - Switzerland - United Kingdom - United States of America

www.st.com