
Low consumption standby implementation with STSPIN32F0 family

Introduction

The diffusion of the Lithium-ion batteries, thanks to their high energy density, extended the concept of portability and cordless to a wide range of products. Power tools, vacuum cleaners and lawn mowers are only a few examples of this trend.

A key requirement of these applications is the low quiescent consumption extending the battery life when the equipment is stored.

This document describes an effective and affordable implementation of this feature using the brushless motor controllers of the STSPIN32F0 family.

1 List of abbreviations

Following is a list of the abbreviations used in this document:

Table 1. List of abbreviations

Abbreviation	Meaning
MCU	Microcontroller Unit
PMOS	P-channel metal-oxide-semiconductor field-effect transistor
NMOS	N-channel metal-oxide-semiconductor field-effect transistor
AMR	Absolute maximum rating

2 Basic principle and proposed solution

The best way to reduce the quiescent consumption to the lowest level possible, is disconnecting the battery from the unused circuitry. This is usually done through a PMOS placed between the battery (source) and the circuitry (drain).

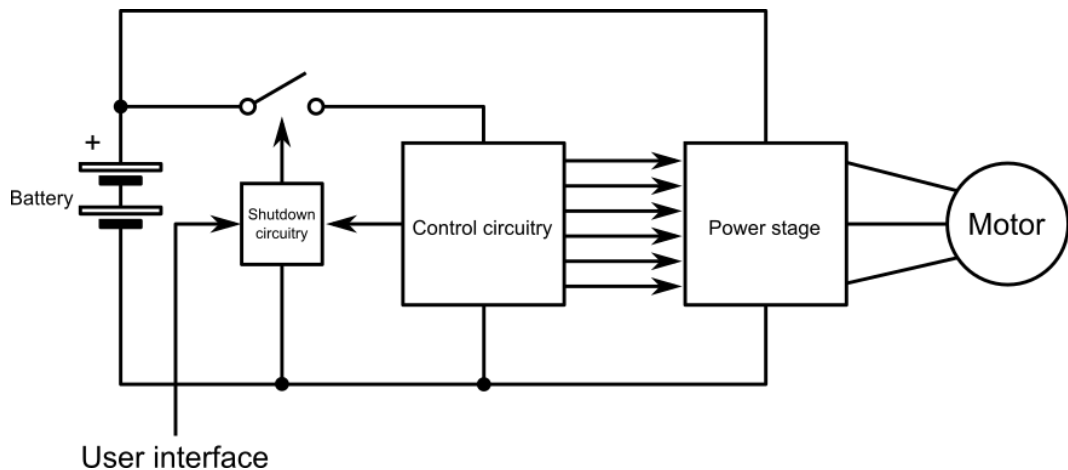
In the proposed solution (see [Figure 1](#)), the disconnected circuitry is the STSPIN32F0 together with all the devices dedicated to the control of the motor (e.g. Hall-effect sensors, encoders, NTC, ...).

On the contrary, the power stage is directly connected to the battery. The main reason is that the current required to drive the motor is typically too high to be managed by a PMOS-based switch.

The key points to be considered during the design of this solution are:

1. The PMOS performing the disconnection must be able to sustain the operating current of the circuitry.
2. Take care of parasitic connections with other circuitries that cannot be disconnected from the battery (e.g. battery monitor, power stage, ...).
3. The PMOS should be disabled by default. It is not a must, but the low-consumption mode is normally considered the idle status of the equipment.

Figure 1. Basic principle block diagram



2.1 Turn-on through external trigger switch

One of the most common ways to enable a battery-supplied tool is through a mechanical switch. As soon as the switch is closed, the tool returns operative and the motor must be driven as required by the control algorithm.

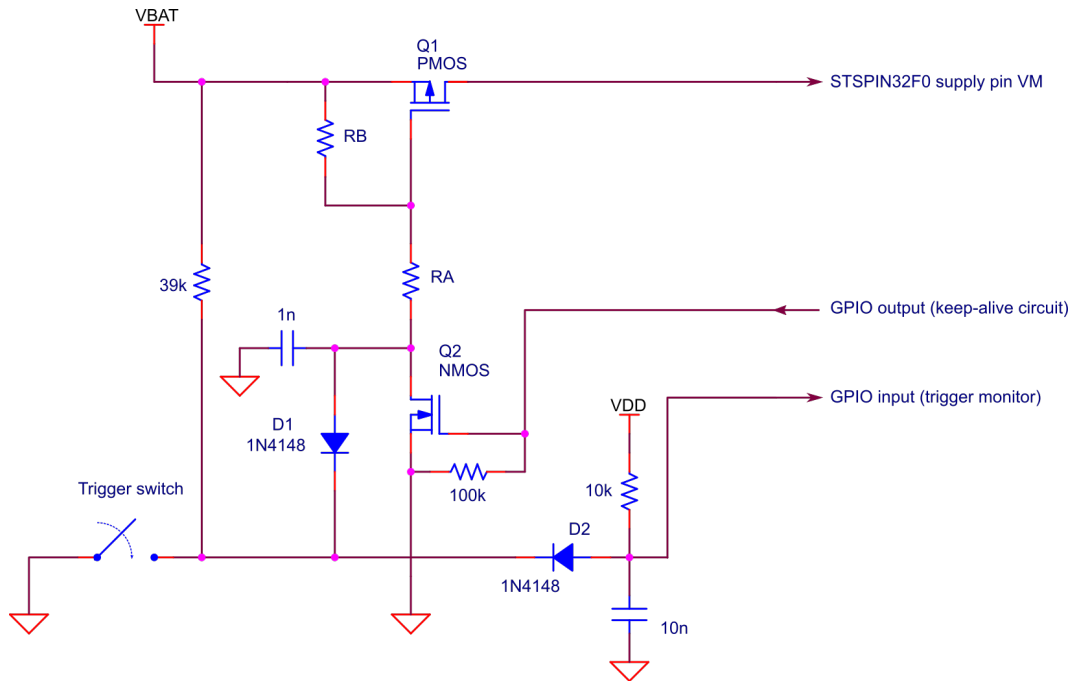
In the proposed schematic of [Figure 2](#) closing the trigger switch, the gate of the PMOS is forced low connecting the battery to the control circuitry. The V_{gs} of the PMOS is calculated by [Eq. \(1\)](#). In order to guarantee a good turn-on of D1 diode, a bias current of 100 μA or more is recommended (see [Eq. \(2\)](#) for an approximated value).

Equation 1

$$V_{gs, Q1} = (V_{F, D1} - V_{BAT}) \frac{R_B}{R_A + R_B} \quad (1)$$

Equation 2

$$I_{F, D1} \sim \frac{V_{BAT}}{R_A + R_B} \quad (2)$$

Figure 2. Turn-on through external trigger switch – schematic example


When the battery voltage is above the absolute rating of the PMOS' V_{gs} (in most cases 20 V), it is safer to use a solution based on Zener diodes (Figure 3). In this case, R_B can be significantly higher than R_A and the V_{gs} is imposed by the Zener voltage of $DZ1$. In this solution it is important to verify that the power dissipation of $DZ1$, R_A and $D1$ are still in a safe operating area (see equations below):

Equation 3

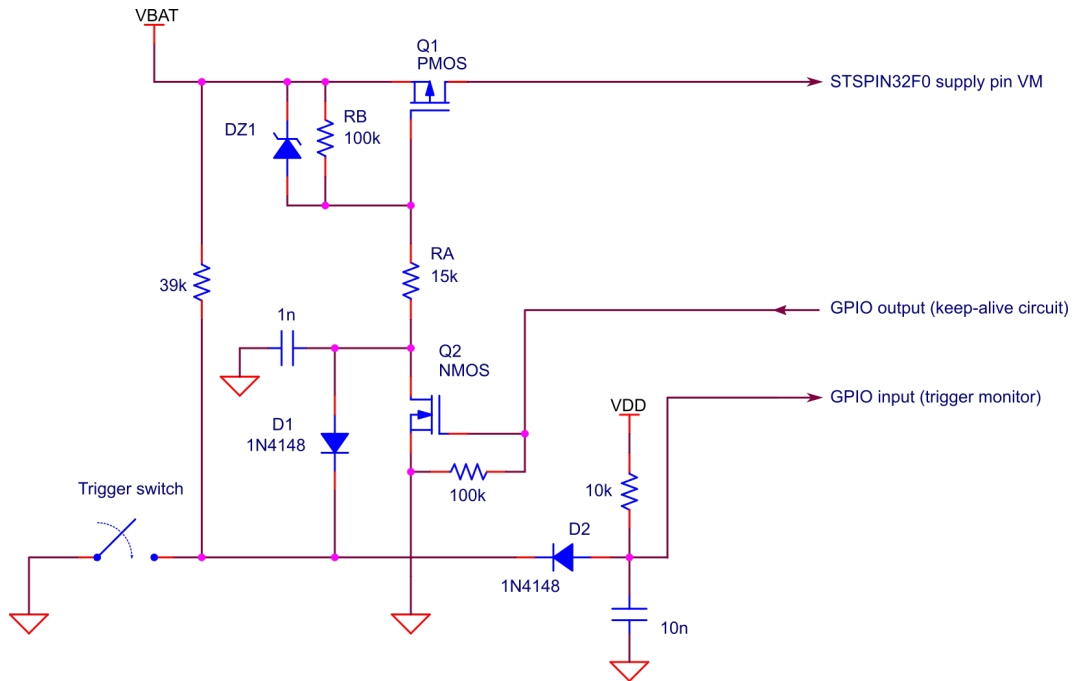
$$P_{d,DZ1} = V_{Z,DZ1} \times I_{Z,DZ1} = V_{Z,DZ1} \times \left(\frac{V_{BAT} - V_{Z,DZ1} - V_{F,D1}}{R_A} - \frac{V_{Z,DZ1}}{R_B} \right) \quad (3)$$

Equation 4

$$P_{d,D1} = V_{F,D1} \times I_{F,D1} = V_{F,D1} \times \left(\frac{V_{BAT} - V_{Z,DZ1} - V_{F,D1}}{R_A} \right) \quad (4)$$

Equation 5

$$P_{d,RA} = \frac{(V_{BAT} - V_{Z,DZ1} - V_{F,D1})^2}{R_A} \quad (5)$$

Figure 3. Turn-on through external trigger switch – schematic example with Zener diode


2.2 Keep-alive circuit

As soon as the PMOS connects the battery to the STSPIN32F0 and the VM rises above the turn-on threshold, the power-up sequence starts, and the integrated buck regulator performs the soft-start ramp supplying the MCU. Details of the above sequence are listed in the datasheet of the devices.

When the MCU is operative, it is possible to keep the PMOS closed using Q2 NMOS. In fact, it acts as an MCU-driven switch in parallel to the external trigger switch.

In this way, the firmware takes control of the connection between the battery and the STSPIN32F0, allowing the code to perform a safe switch-off, for example, braking the motor.

Table 2. Q2 NMOS key requirements

Symbol	Characteristic	Recommended value
VDS,max	Drain-source maximum voltage	$\geq 1.2 \times \text{VBAT}$
VGS(th)	Gate-source threshold voltage	$\leq 2.5 \text{ V}$

It is recommended to set this GPIO output at the very beginning of the MCU's initialization.

2.3 Detection of external trigger switch status

While the STSPIN32F0 is kept supplied by the keep-alive circuit (see [Section 2.2](#)), the actual status of the external trigger switch must be constantly monitored in order to execute the shut-down sequence when it is released.

In the proposed circuit, the monitoring GPIO is connected to the switch through the D2 diode.

As long as the switch is closed, the GPIO is forced low through D2. Releasing the switch, D2 turns off and the GPIO is pulled up by the resistor. A strong filtering of the signal is recommended.

3 Protection against reverse biasing from power stage outputs

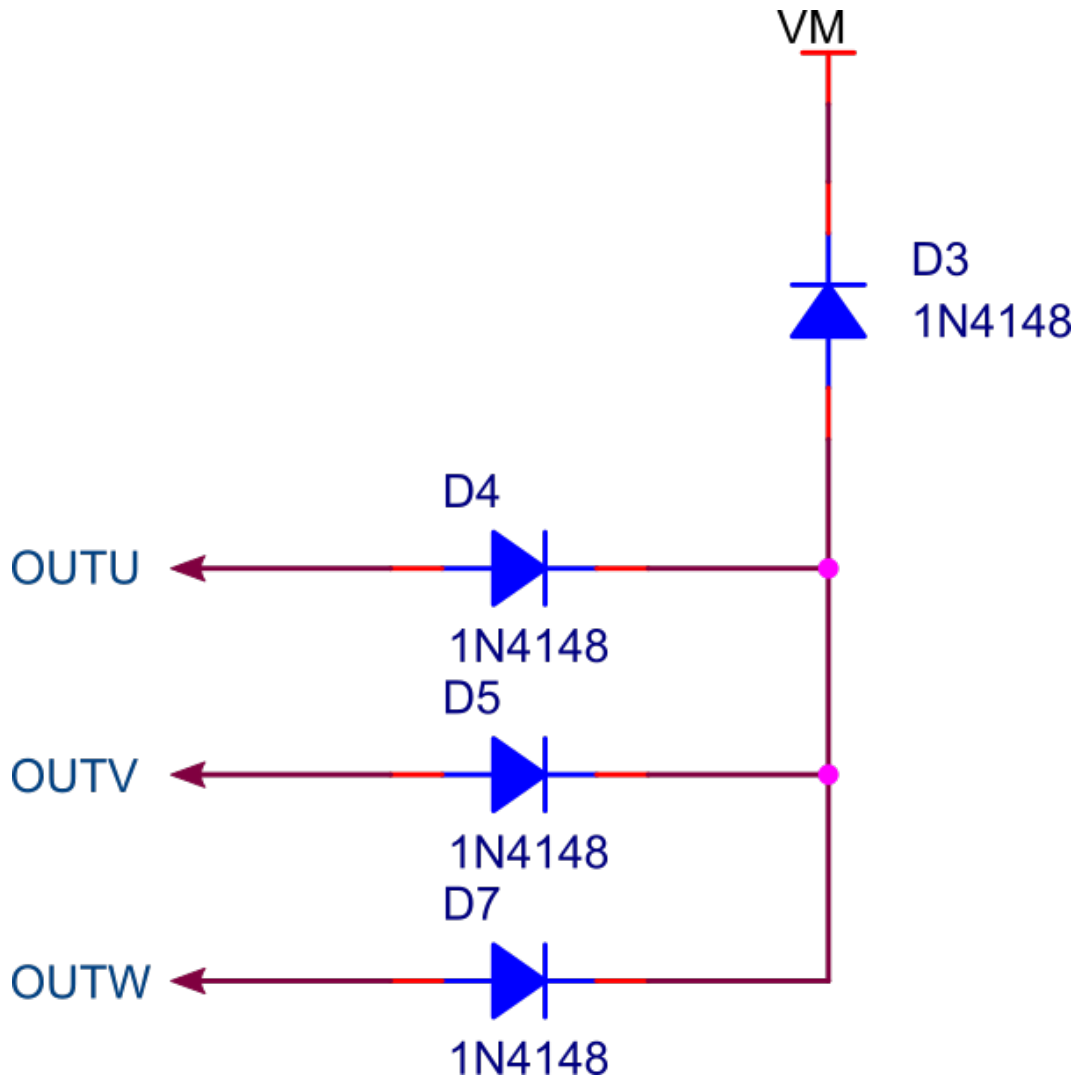
As shown in the block diagram of [Figure 1](#), the battery is always connected to the power stage while the control side is disconnected through the PMOS switch. In this way, the voltage of the power stage outputs (V_{OUT}) can be higher than the control logic supply (V_M) violating the AMR limit of the gate driving circuitry: $V_{OUT,max} = V_M + 2 V$. The device can be protected against this condition by adding protection diodes between each output and the V_M supply, as shown in [Figure 4](#).

The circuit imposes the [Eq. \(6\)](#) condition keeping the device within AMR. During normal operation the diodes are always off.

Equation 6

$$MAX(V_{OUTx} - V_M) = 2 \times V_F \cong 1.2 V$$

(6)

Figure 4. Protection circuit


Revision history

Table 3. Document revision history

Date	Version	Changes
5- Nov-2019	1	Initial release.

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